



dei-ug

RADIO FREQUENCY CRABBING SYSTEM FOR AN ELECTRON-ION COLLIDER

ALEJANDRO CASTILLA

September 13th 2012

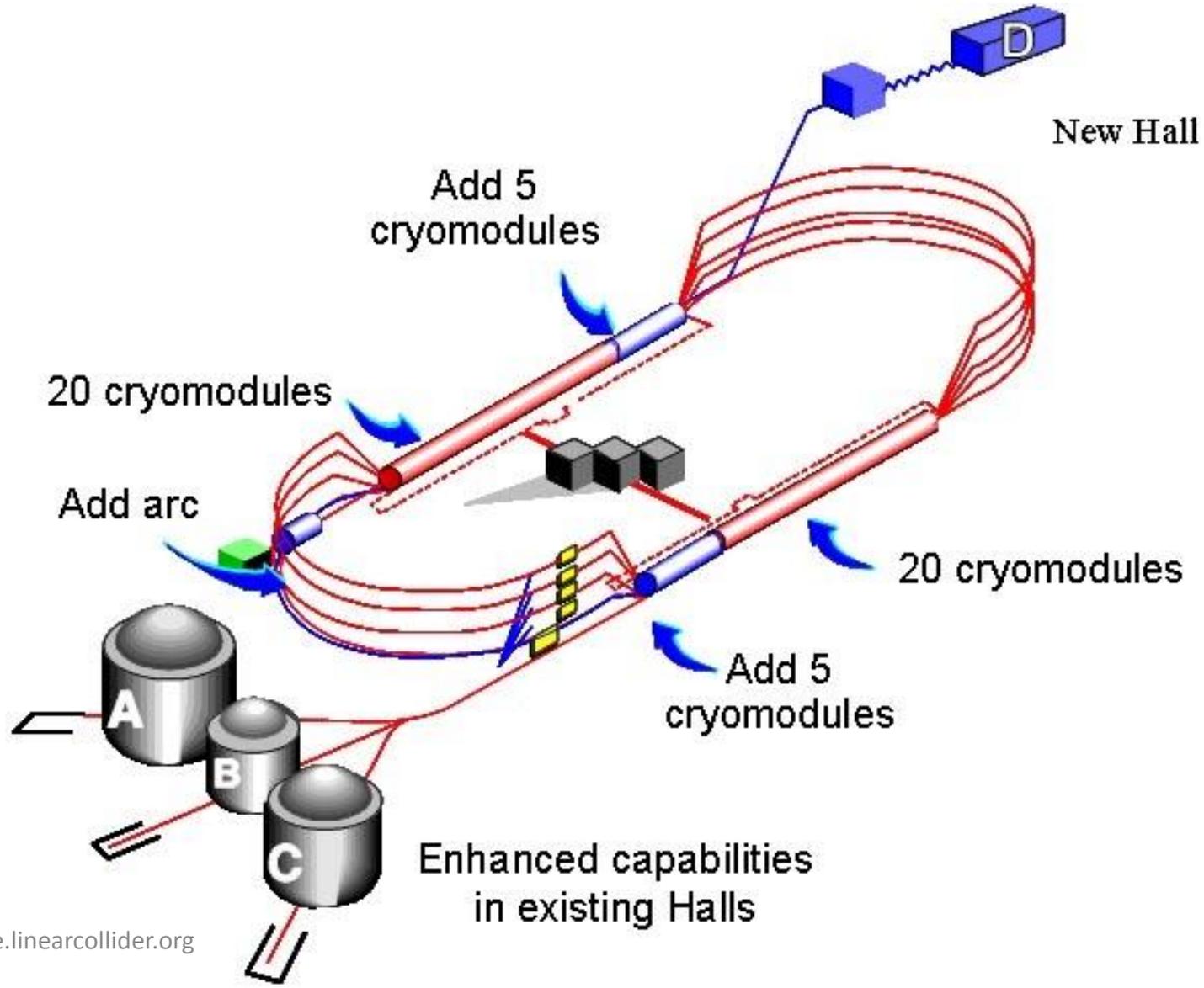


Outline

- **Thomas Jefferson National Laboratory:**
 - JLab and the 12 GeV Upgrade.
 - The Medium-energy Electron-Ion Collider.
- **Improving Luminosity on Colliders (Crabbing):**
 - The Idea behind Radio-Frequency Crabbing Systems.
 - Our Design.
- **Next Generation X-Ray Sources:**
 - Inverse Compton Scattering.
 - Cubix (MIT/Jlab).

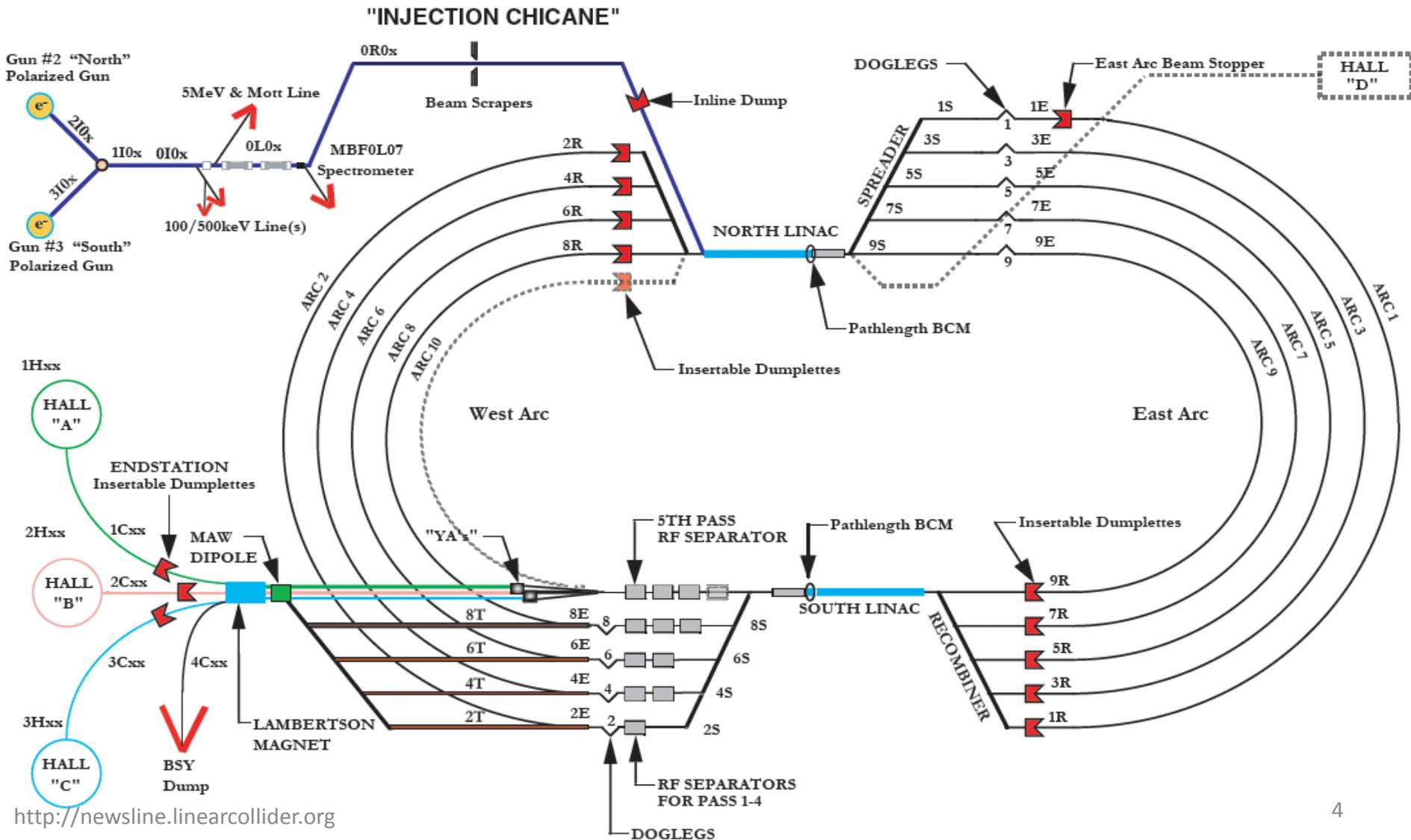


JLab 12 GeV Upgrade



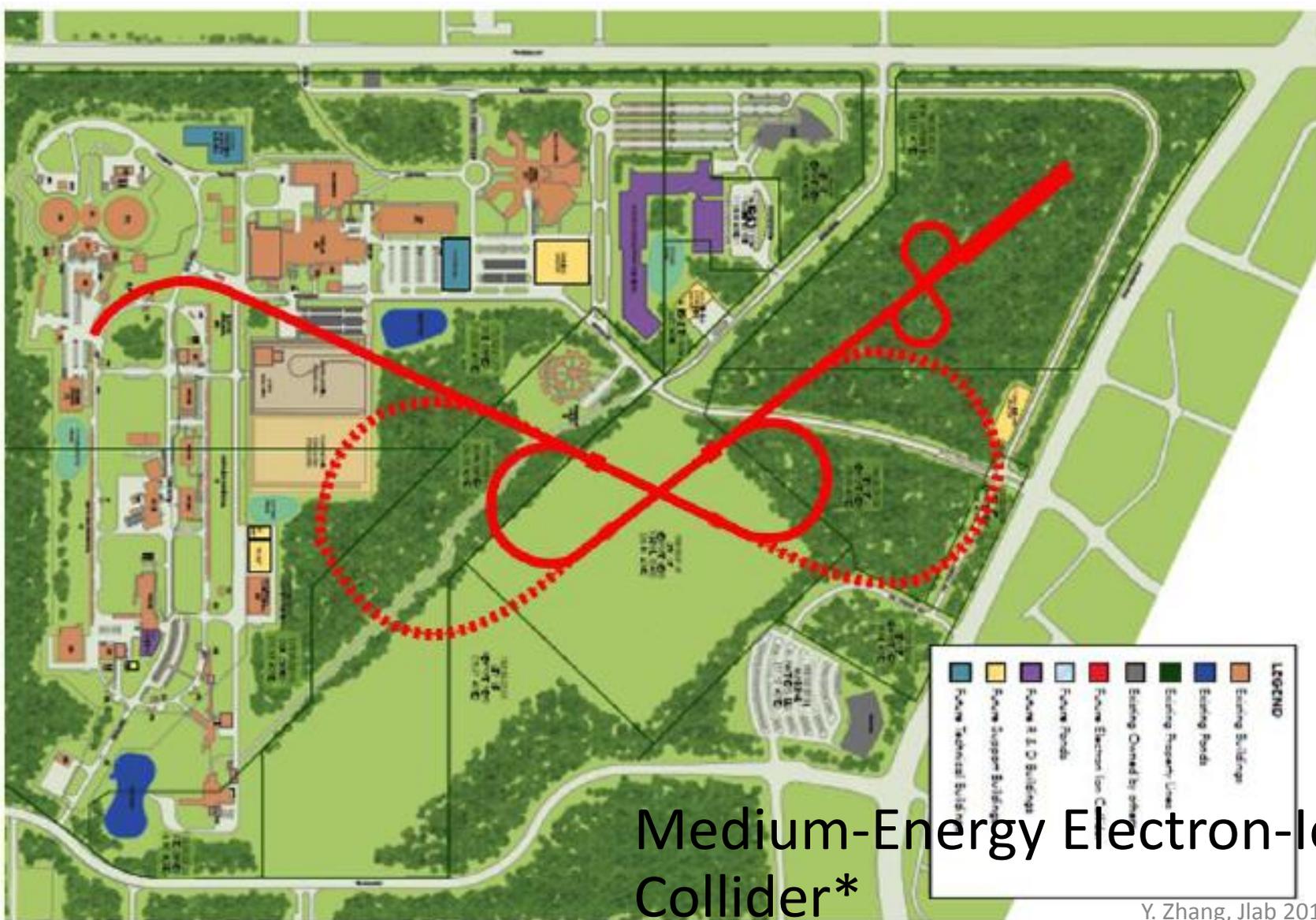


JLab 12 GeV Upgrade





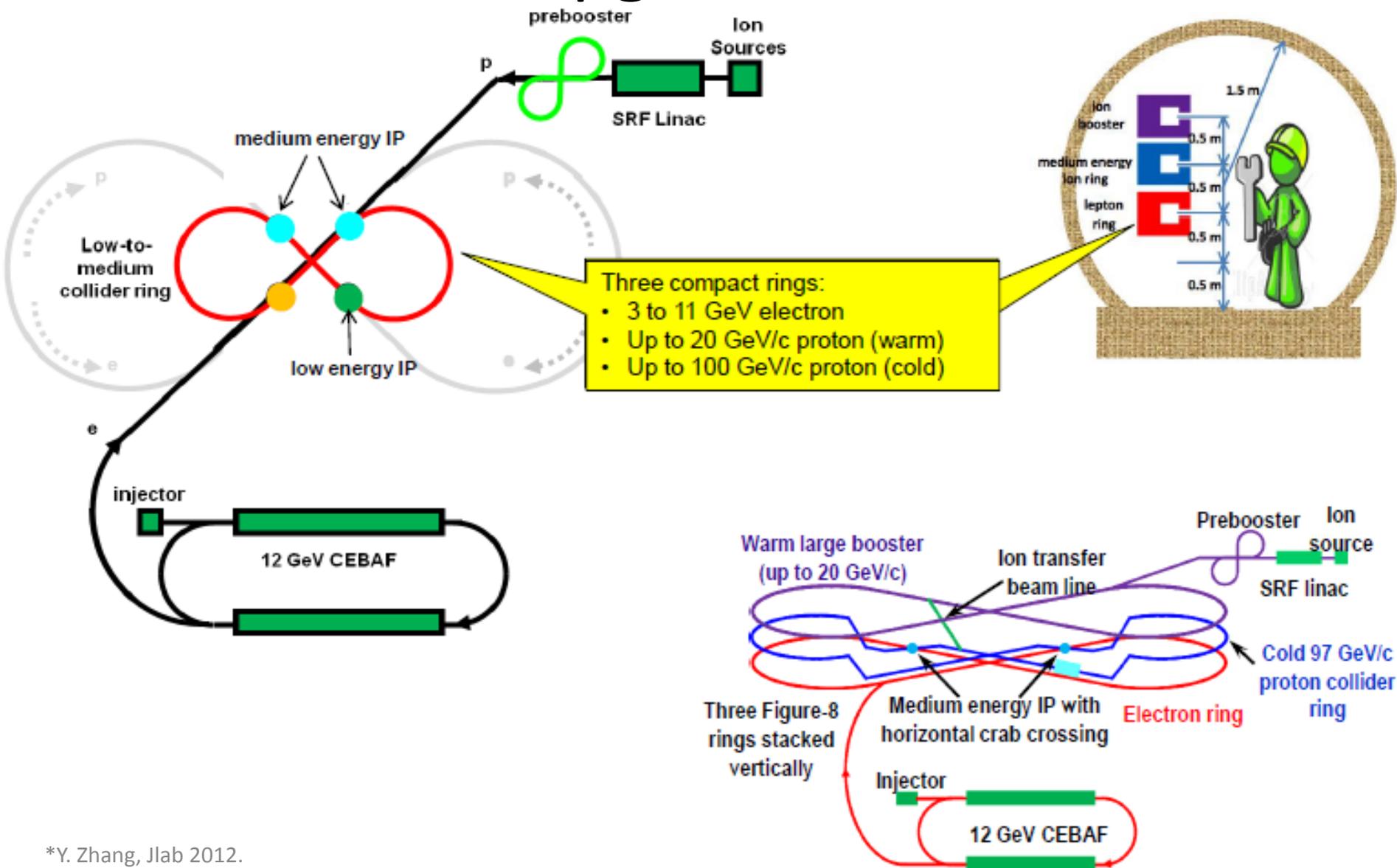
deci-ug Jlab 12 GeV Upgrade and the MEIC*



Medium-Energy Electron-Ion Collider*



Jlab 12 GeV Upgrade and the MEIC*

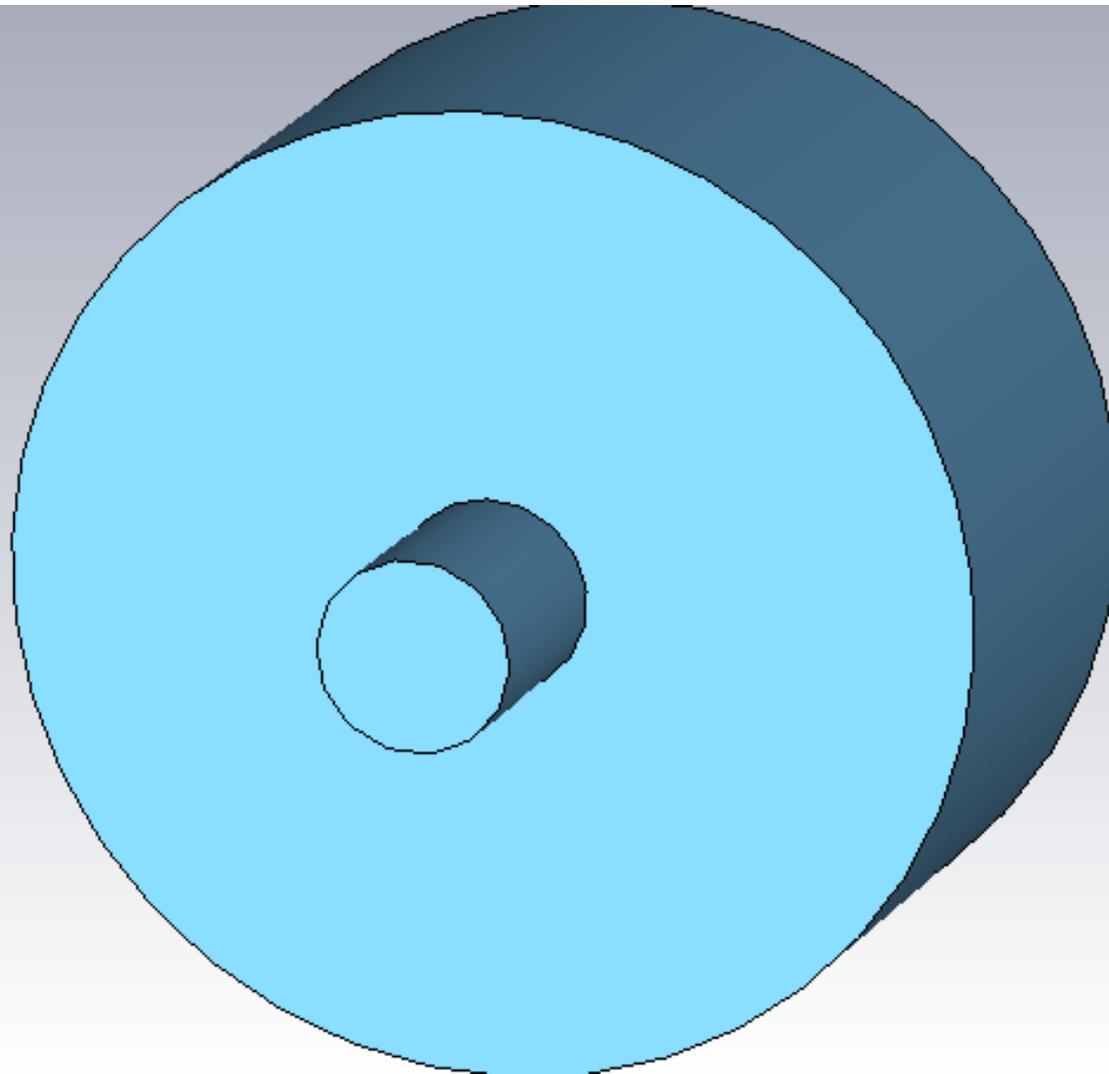


*Y. Zhang, Jlab 2012.



Electromagnetic Resonators

- **Perfect conductor: Pillbox.**



Electromagnetic Resonators

Electric field

$$\nabla \times (\nabla \times \vec{E}) = i\omega \nabla \times \vec{B}$$

$$\nabla (\nabla \cdot \vec{E}) - \nabla^2 \vec{E} = \mu\epsilon\omega^2 \vec{E}$$

$$\nabla \times \vec{B} = -i\mu\epsilon\omega \vec{E}$$

$$\nabla \cdot \vec{E} = 0$$

$$\nabla^2 \vec{E} + \mu\epsilon\omega^2 \vec{E} = 0$$

Magnetic field

$$\nabla \times (\nabla \times \vec{B}) = -i\mu\epsilon\omega \nabla \times \vec{E}$$

$$\nabla (\nabla \cdot \vec{B}) - \nabla^2 \vec{B} = \mu\epsilon\omega^2 \vec{E}$$

$$\nabla \times \vec{B} = -i\mu\epsilon\omega \vec{E}$$

$$\nabla \cdot \vec{E} = 0$$

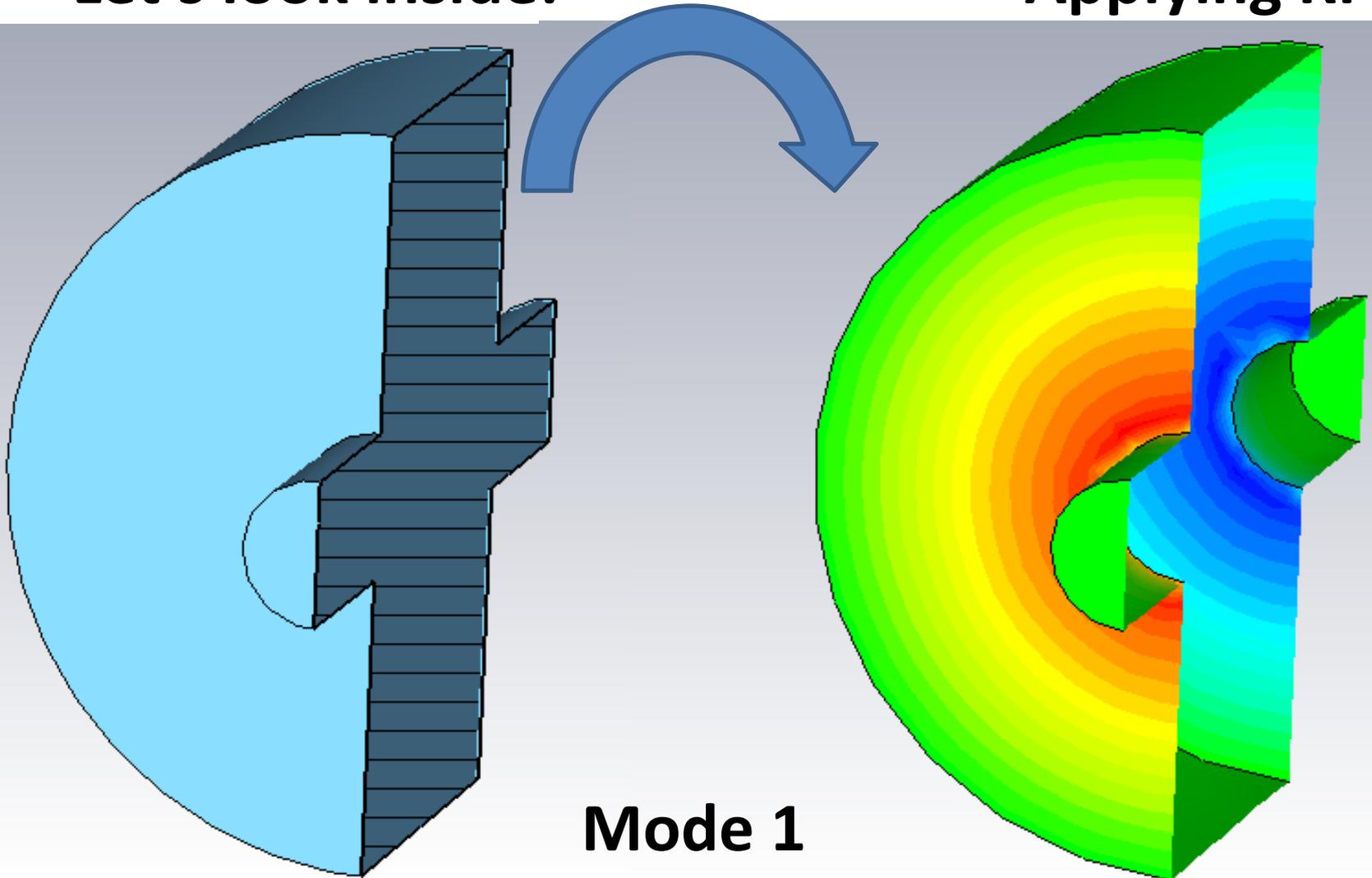
$$\nabla^2 \vec{B} + \mu\epsilon\omega^2 \vec{B} = 0$$

Helmholz equations.

Electromagnetic Resonators

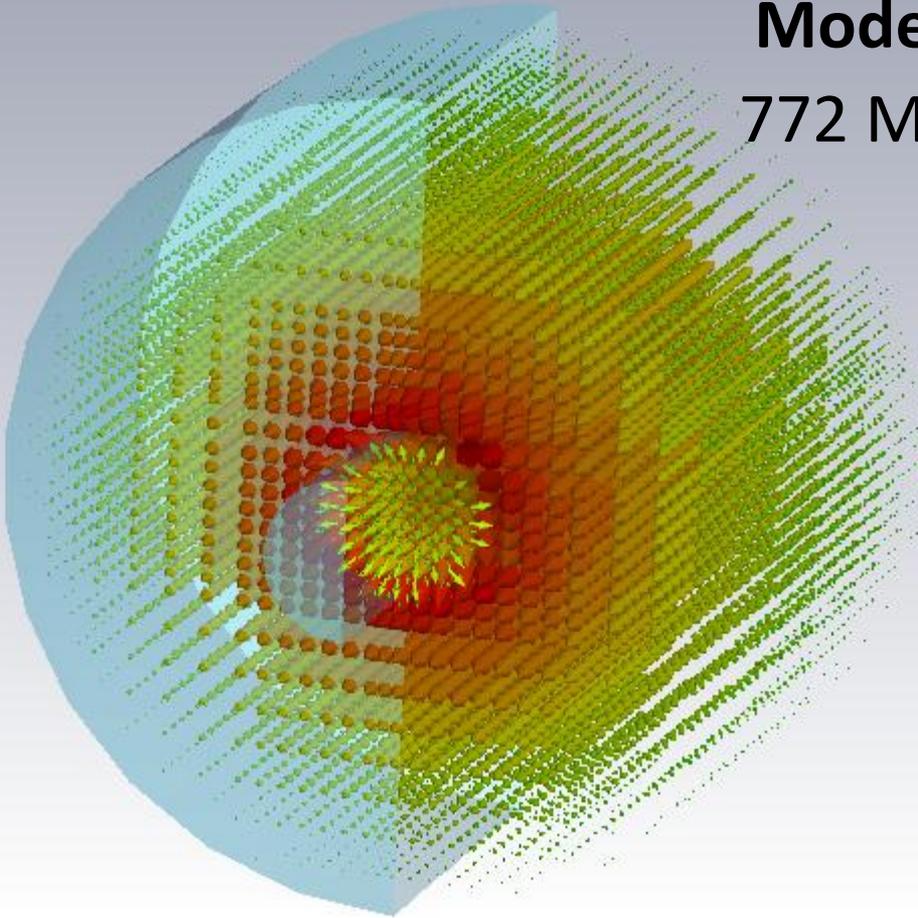
- Let's look inside:

- Applying RF:

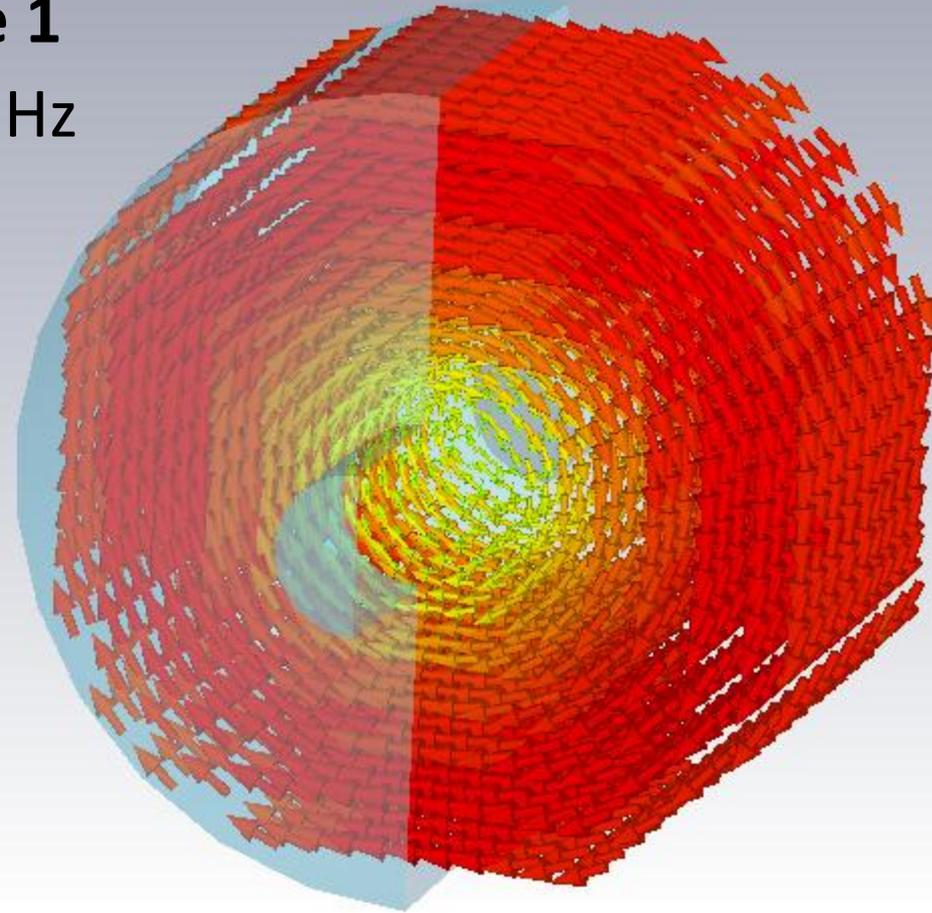


Electromagnetic Resonators

Mode 1
772 MHz



– Electric Field

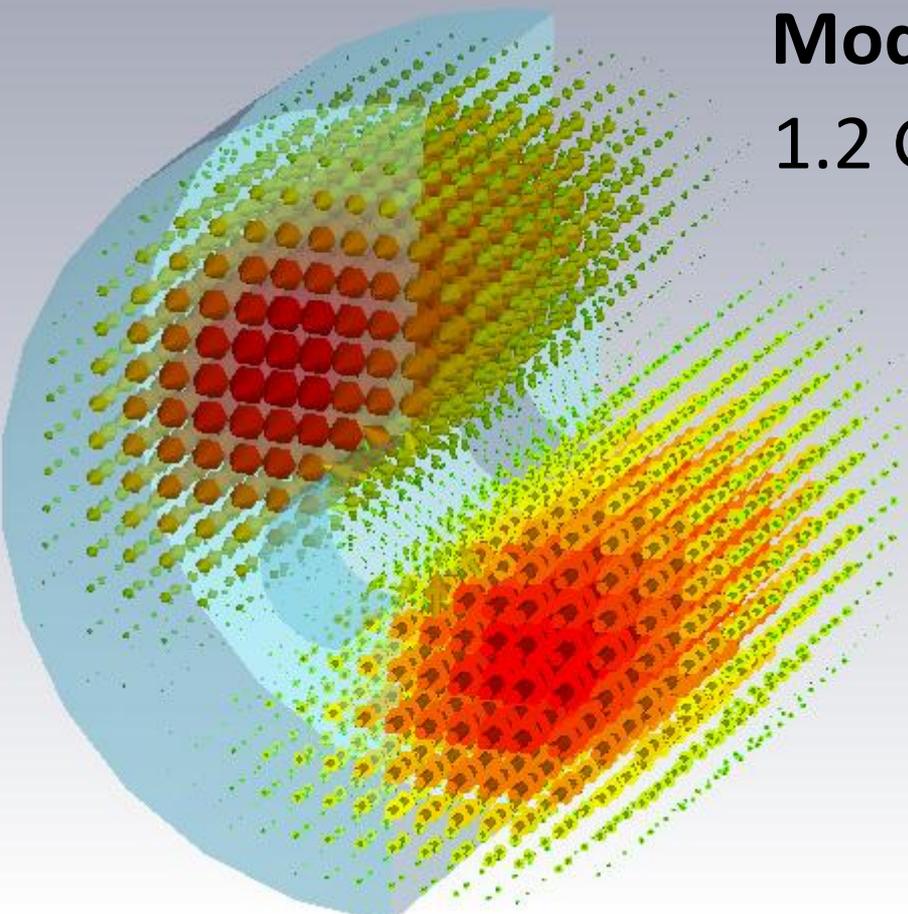


– Magnetic Field

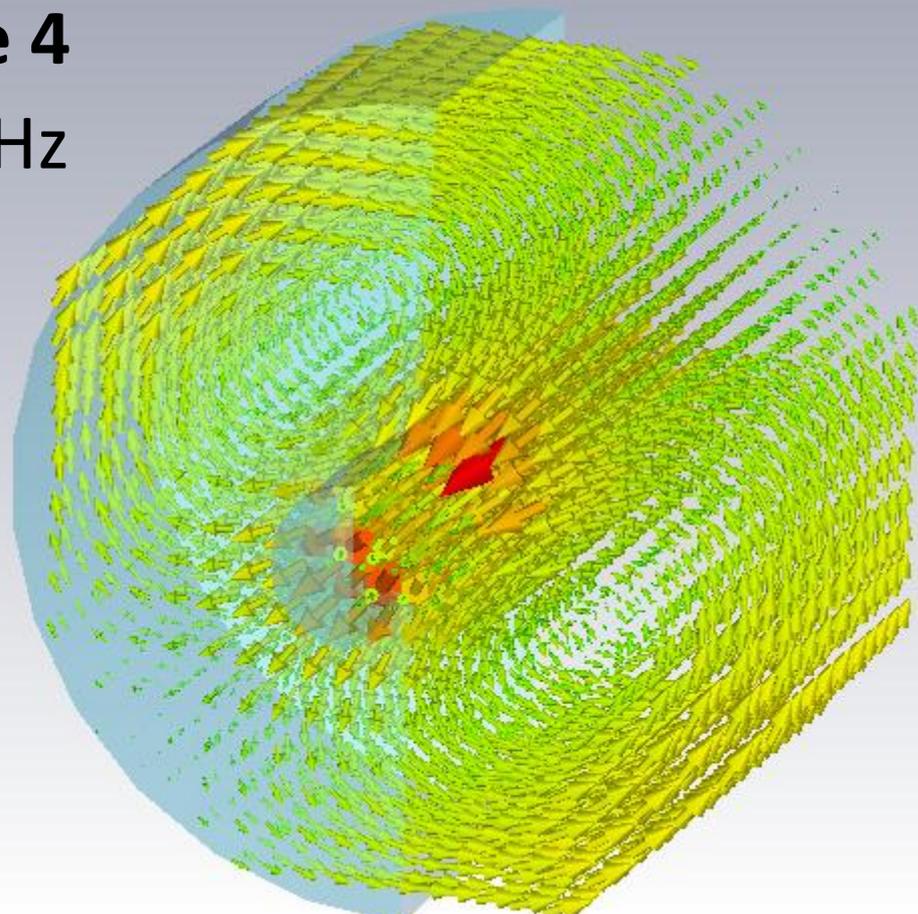
Electromagnetic Resonators

Mode 4

1.2 GHz



– Electric Field



– Magnetic Field

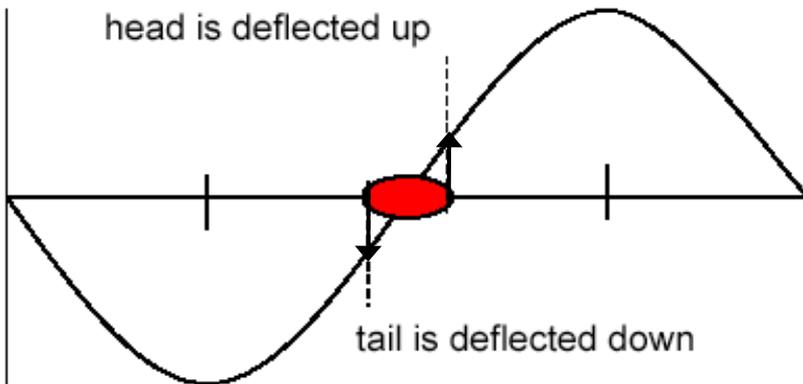
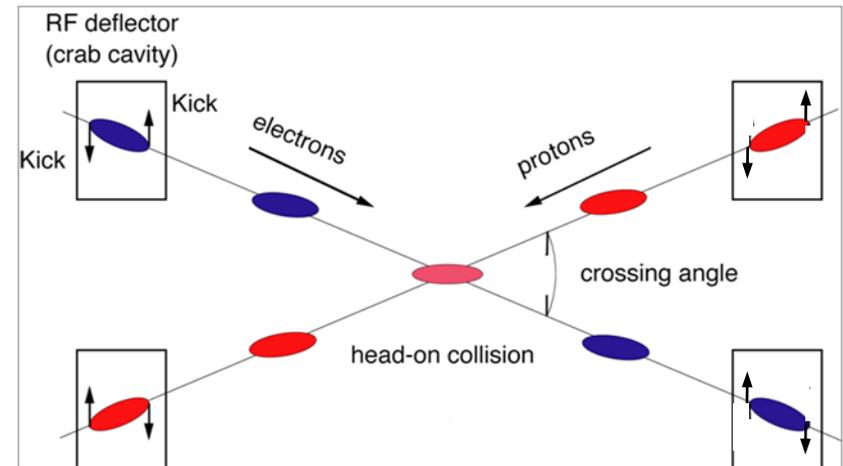
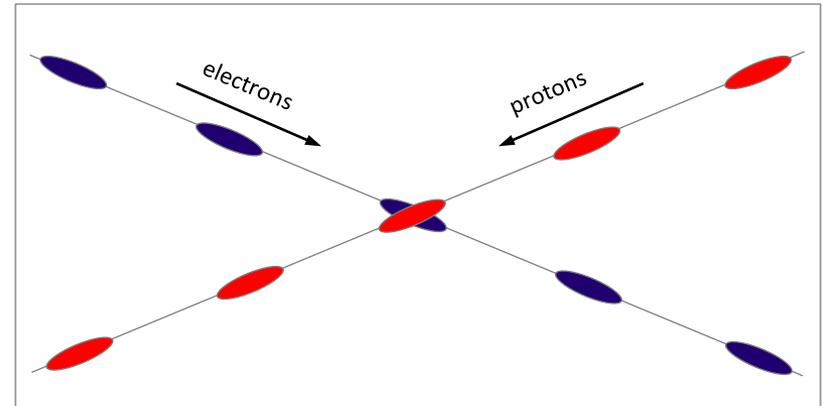
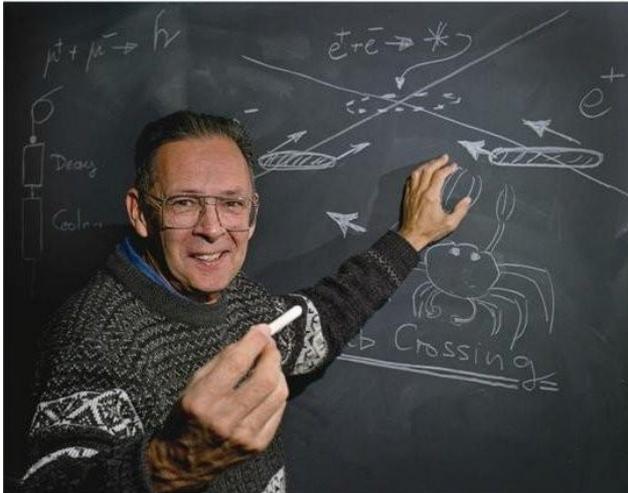
Particle Accelerators

- Particle accelerators propel charged particles using electromagnetic fields.
- Lorentz Force: $\vec{F} = \frac{d\vec{p}}{dt} = q[\vec{E} + \vec{v} \times \vec{B}]$
 - Electric field for acceleration.
 - Magnetic field for bending and focusing.
- Transverse force due the fields as well:

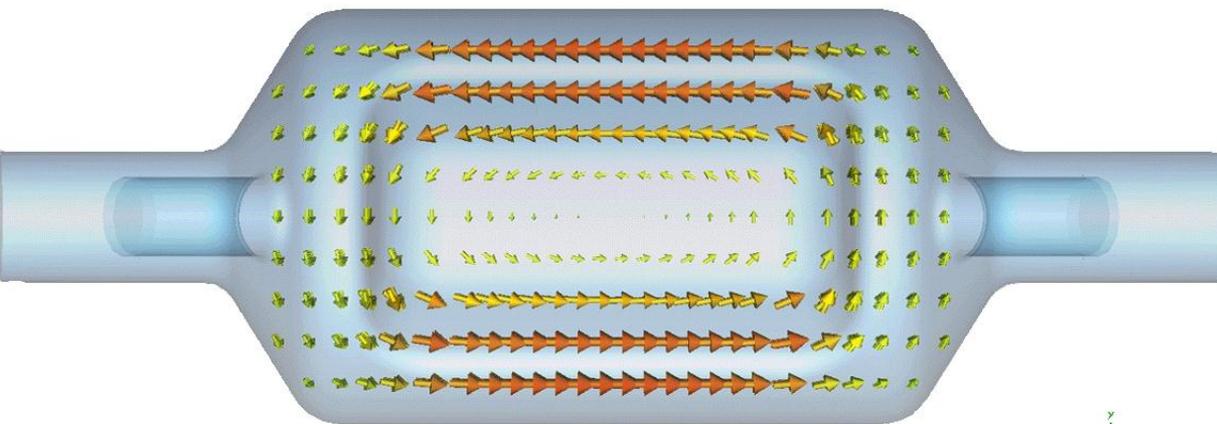
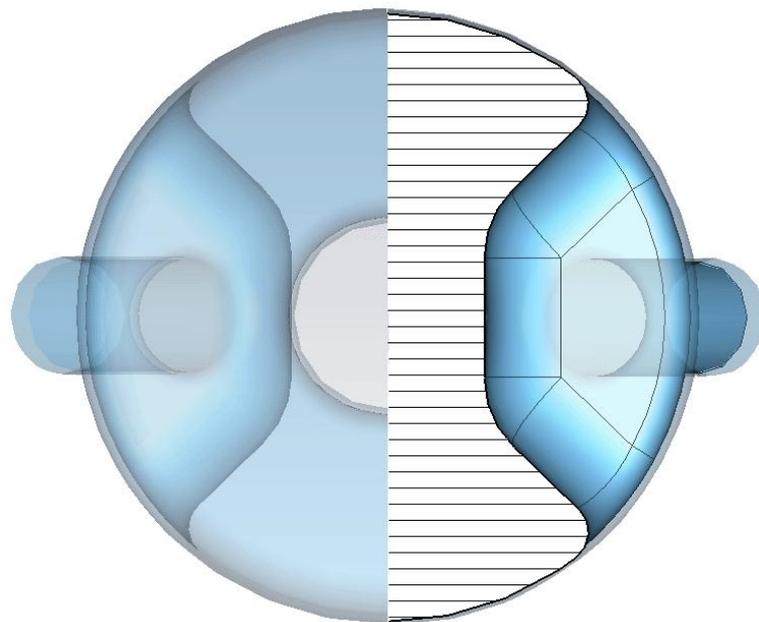
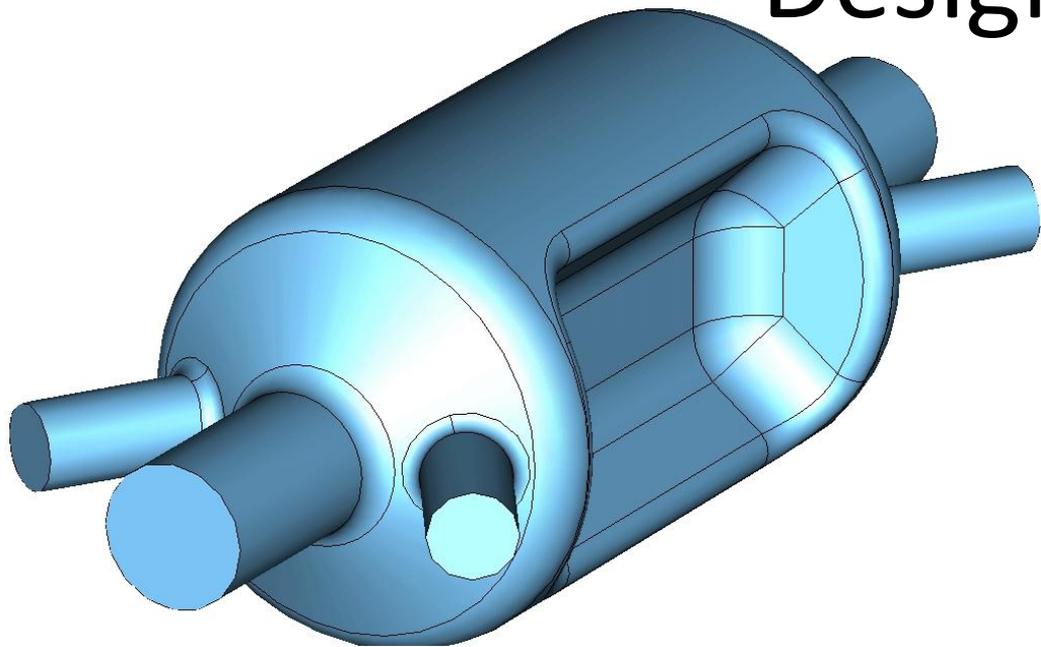
$$V_T = \left| \int_{-\infty}^{\infty} [\vec{E}_T(z) + i(\vec{v} \times \vec{B}(z))_T] e^{\frac{i\omega z}{c}} dz \right|$$

$$V_T = \frac{-i}{\omega/c} \nabla_T V_Z = \frac{-i}{\omega/c} \frac{1}{r_0} \left| \int_{-\infty}^{\infty} \vec{E}_Z(r_0, z) e^{\frac{i\omega z}{c}} dz \right|$$

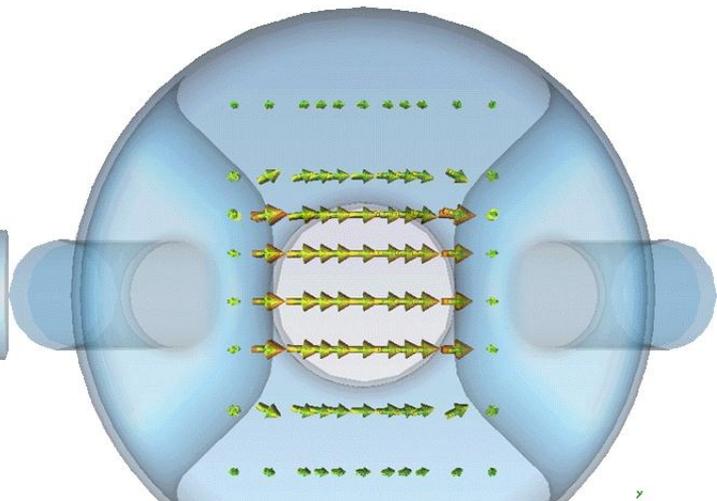
Crabbing Concept



Design



Magnetic Field

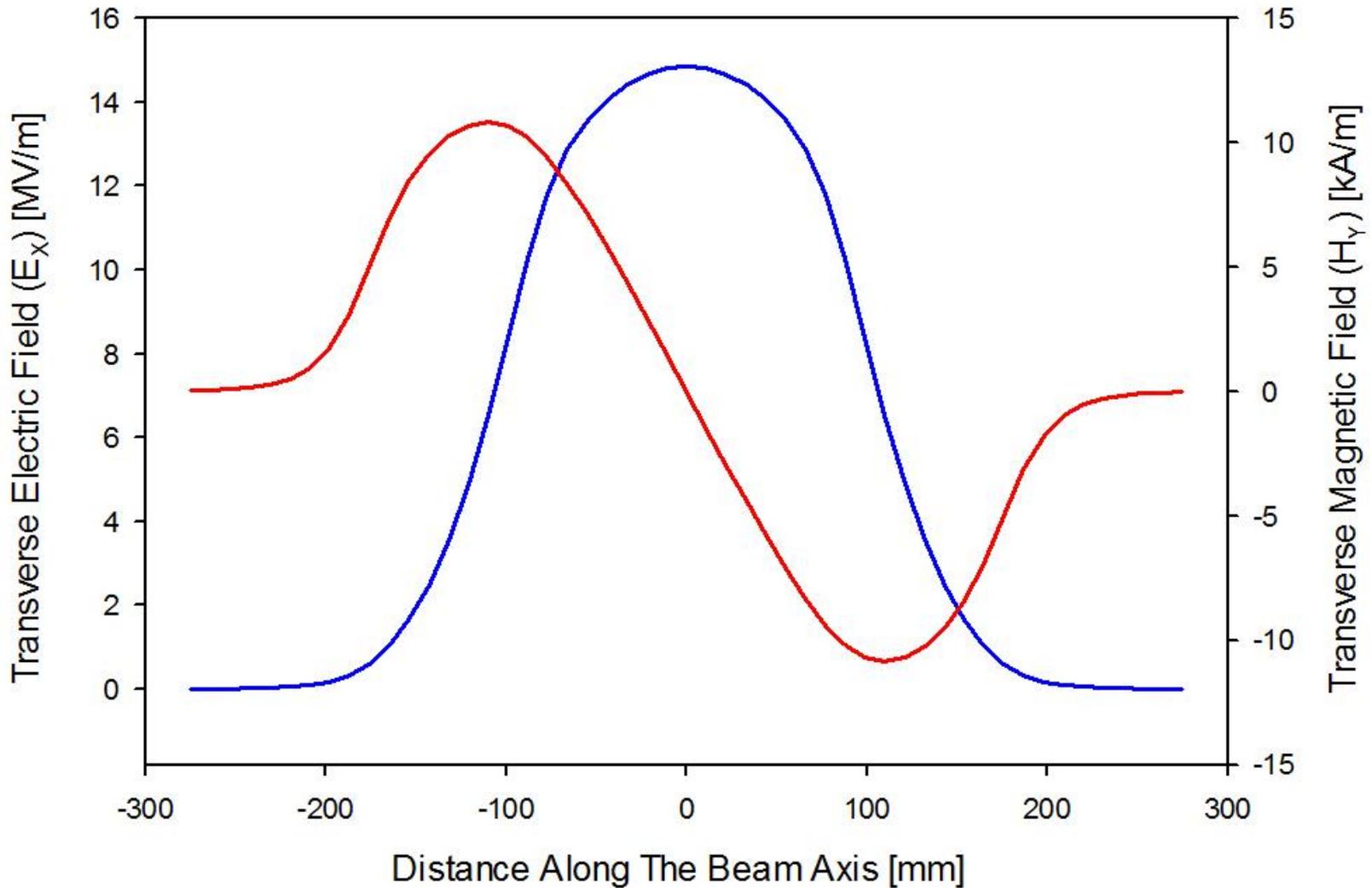


Electric Field¹⁴

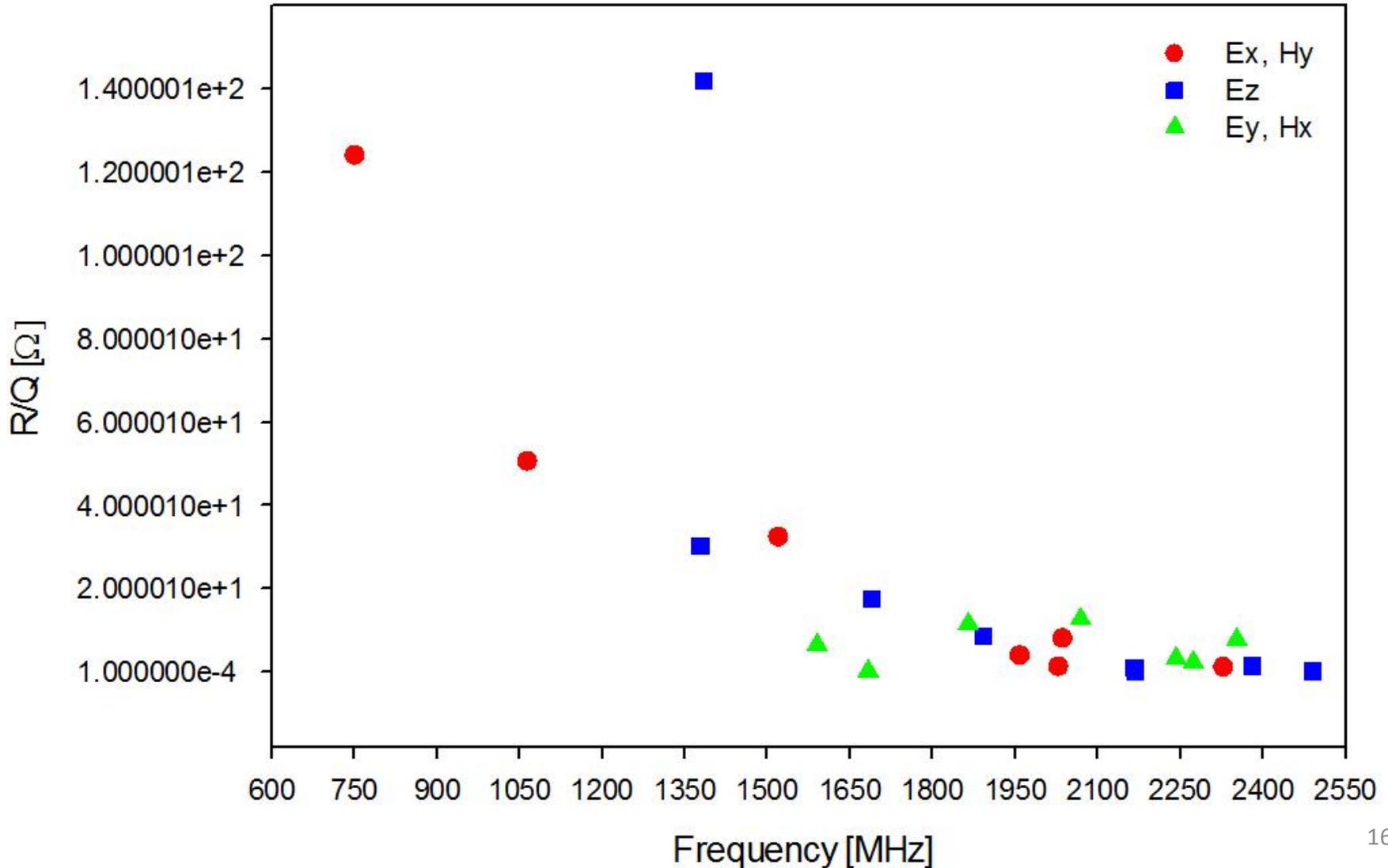


Transverse Fields

(Fundamental Mode)



Higher Order Modes





Assembling





For Electron-Welding



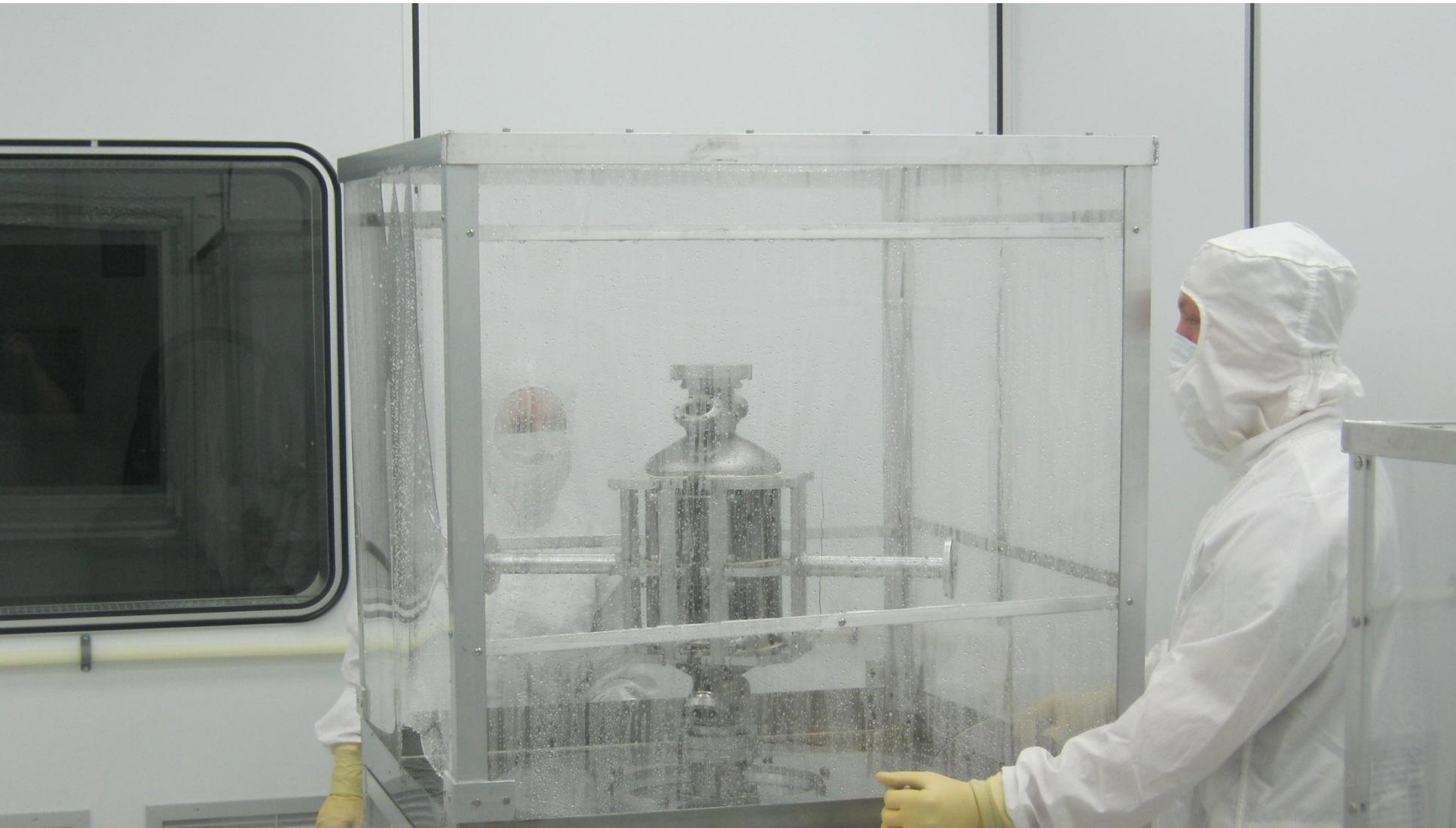


Buffer Chemical Polishing



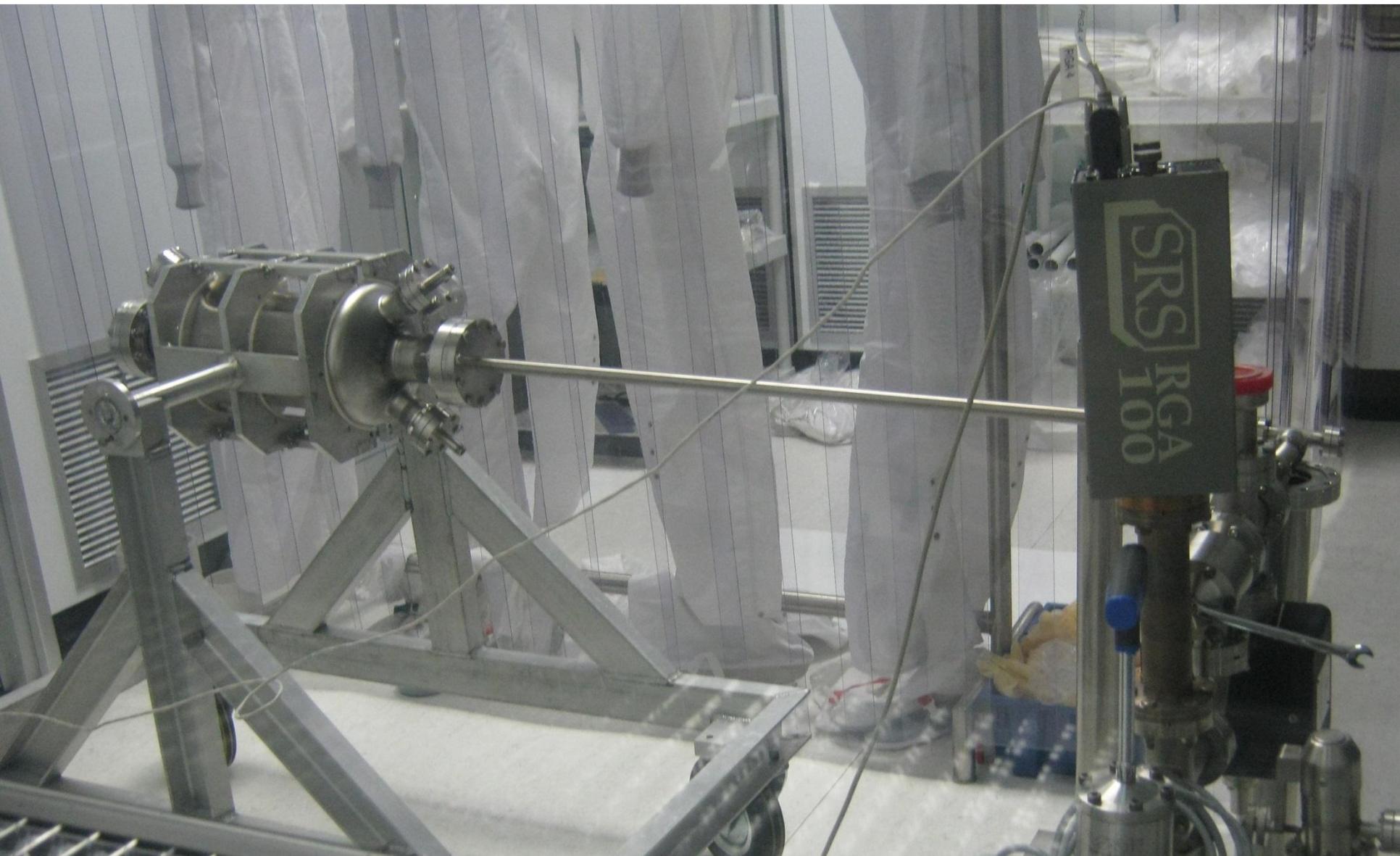


High Pressure Rinsing



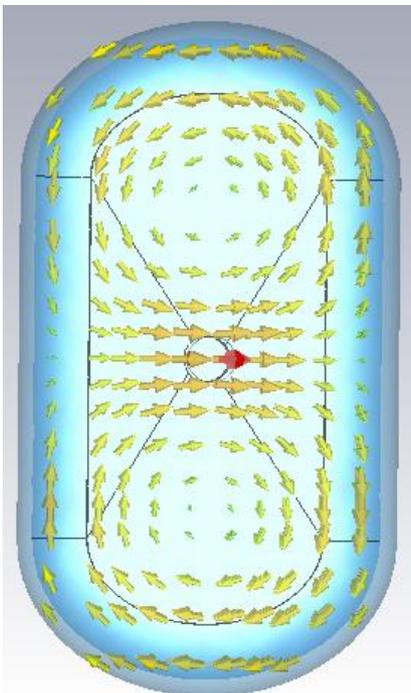


Vacuum Pumping



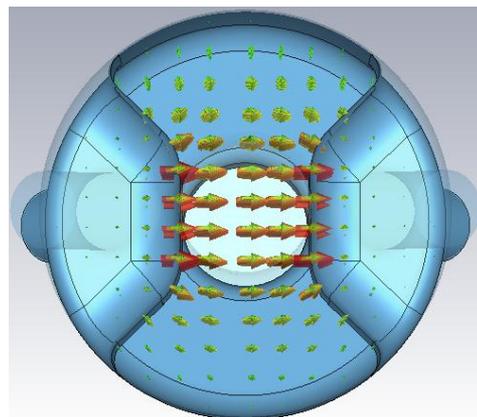
Comparing Crabs

KeK



Parameter	750 MHz	KEK ^[4] MHz	Units
Freq. of π mode	750.1	501.7	MHz
$\lambda/2$ of π mode	200.0	299.8	mm
Freq. of 0 mode	1350.6	~700.0	MHz
Cavity length	300.0	299.8	mm
Cavity width	190.1	866.0	mm
Cavity height	190.1	483.0	mm
Bars width	67.0	-	mm
Angle	45	-	deg
Aperture diameter	60.0	130.0	mm
Deflecting voltage (V_T^*)	0.200	0.300	MV
Peak electric field (E_P^*)	4.45	4.36	MV/m
Peak magnetic field (B_P^*)	9.31	12.45	mT
Geometrical factor	131.4	220	Ω
$[R/Q]_T$	124.15	46.70	Ω
$R_T R_S$	1.65×10^4	1.03×10^4	Ω^2

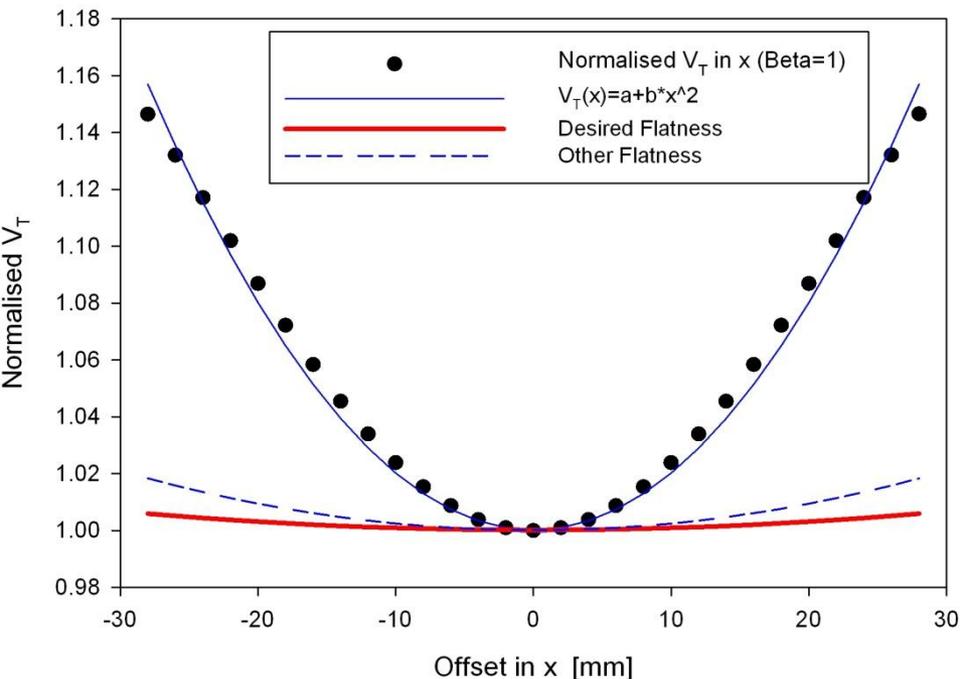
At $E_T^* = 1$ MV/m



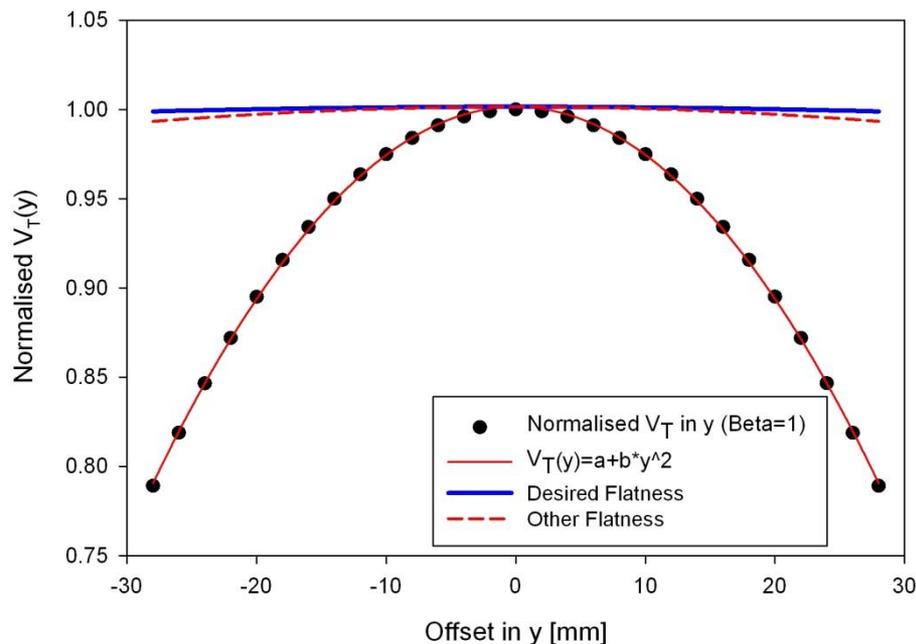
ODU-JLab

Field Uniformity and Emittance

Transverse kick $V_T(x)$ along the x-axis

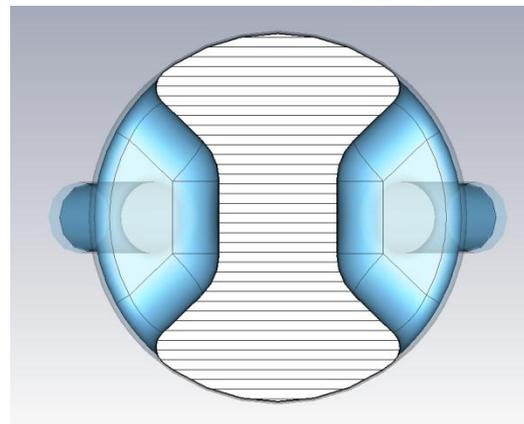


Transverse kick $V_T(y)$ along the y-axis



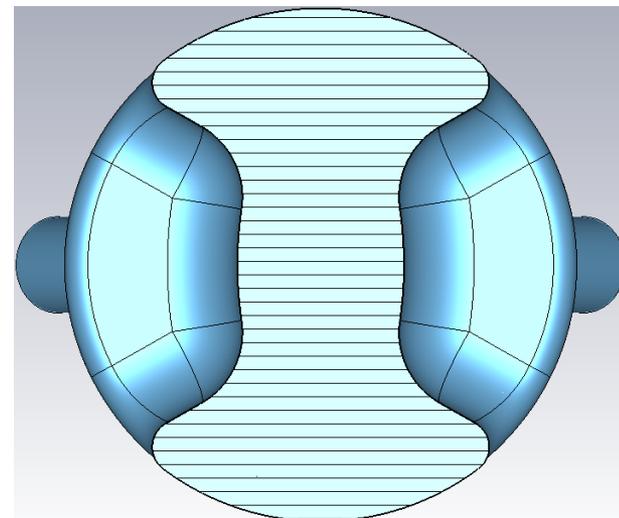
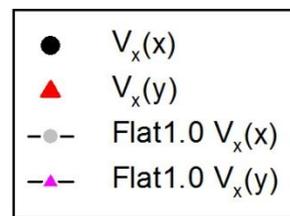
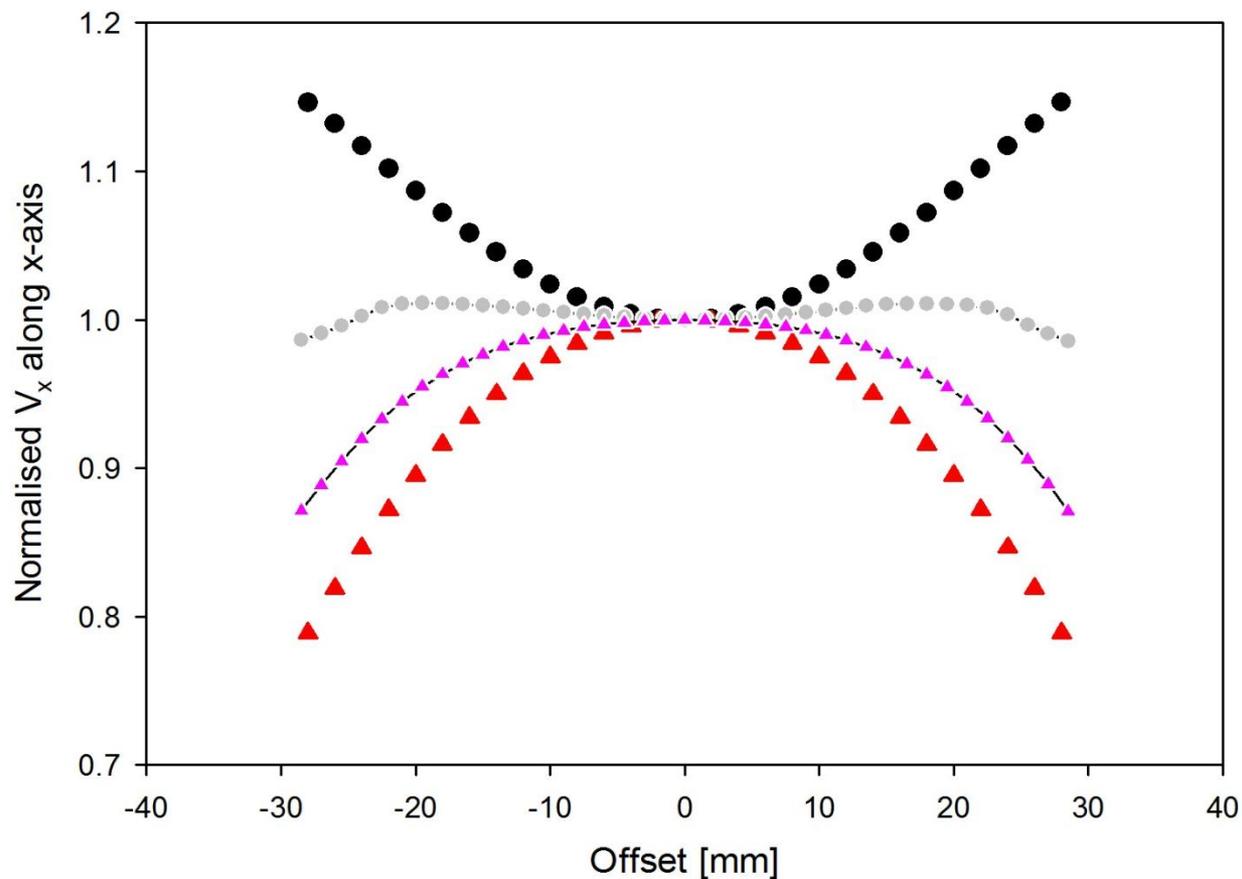
$$\epsilon_{n,rms}^2 \equiv \epsilon_{0n,rms}^2 + \frac{x_{0,rms}^2 (\overline{\Delta p_x^2} - \overline{\Delta p_x}^2)}{m^2 c^2}$$

Therefore, if the proton beam enters the crab cavity with $\epsilon_{0n,rms}(x) = 0.35 \mu\text{m} - \text{rad}$ then comes out of the cavity with $\epsilon_{n,rms}(x) = 0.36 \mu\text{m} - \text{rad}$ after 1 pass. While for the y direction if $\epsilon_{0n,rms}(y) = 0.07 \mu\text{m} - \text{rad}$ then comes out of the cavity with $\epsilon_{n,rms}(y) = 0.13 \mu\text{m} - \text{rad}$ after 1 pass, both considering zero offset.

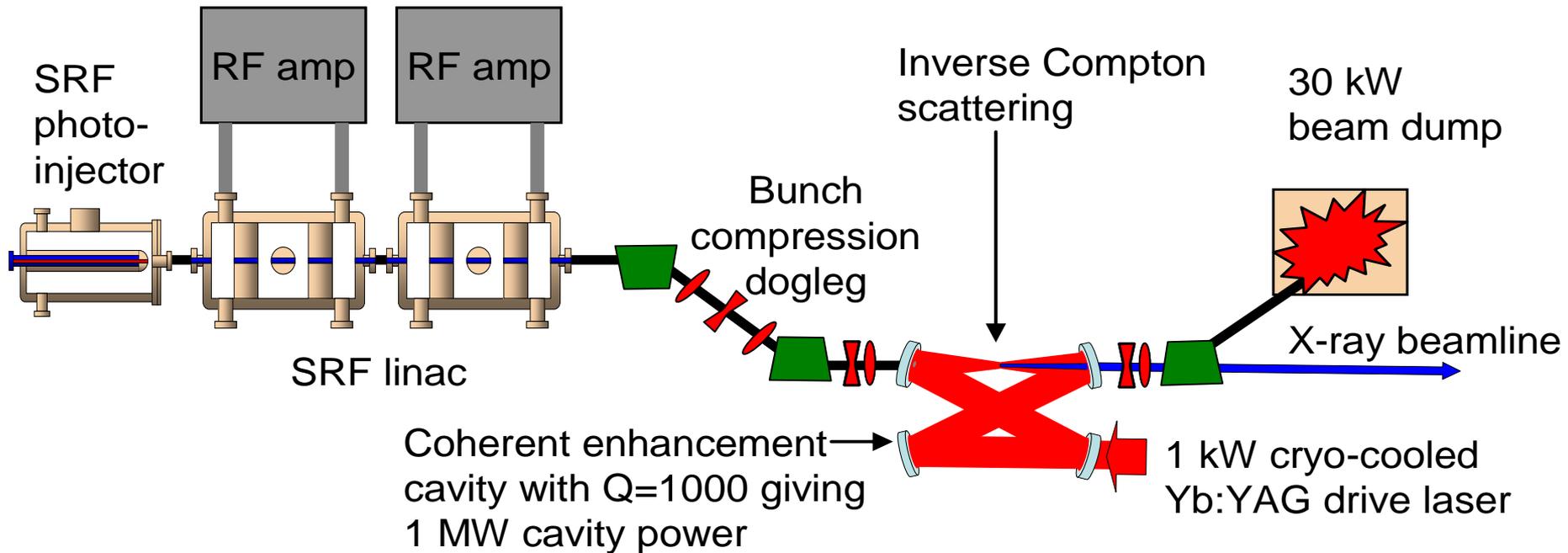


Correcting Field Non-Uniformity

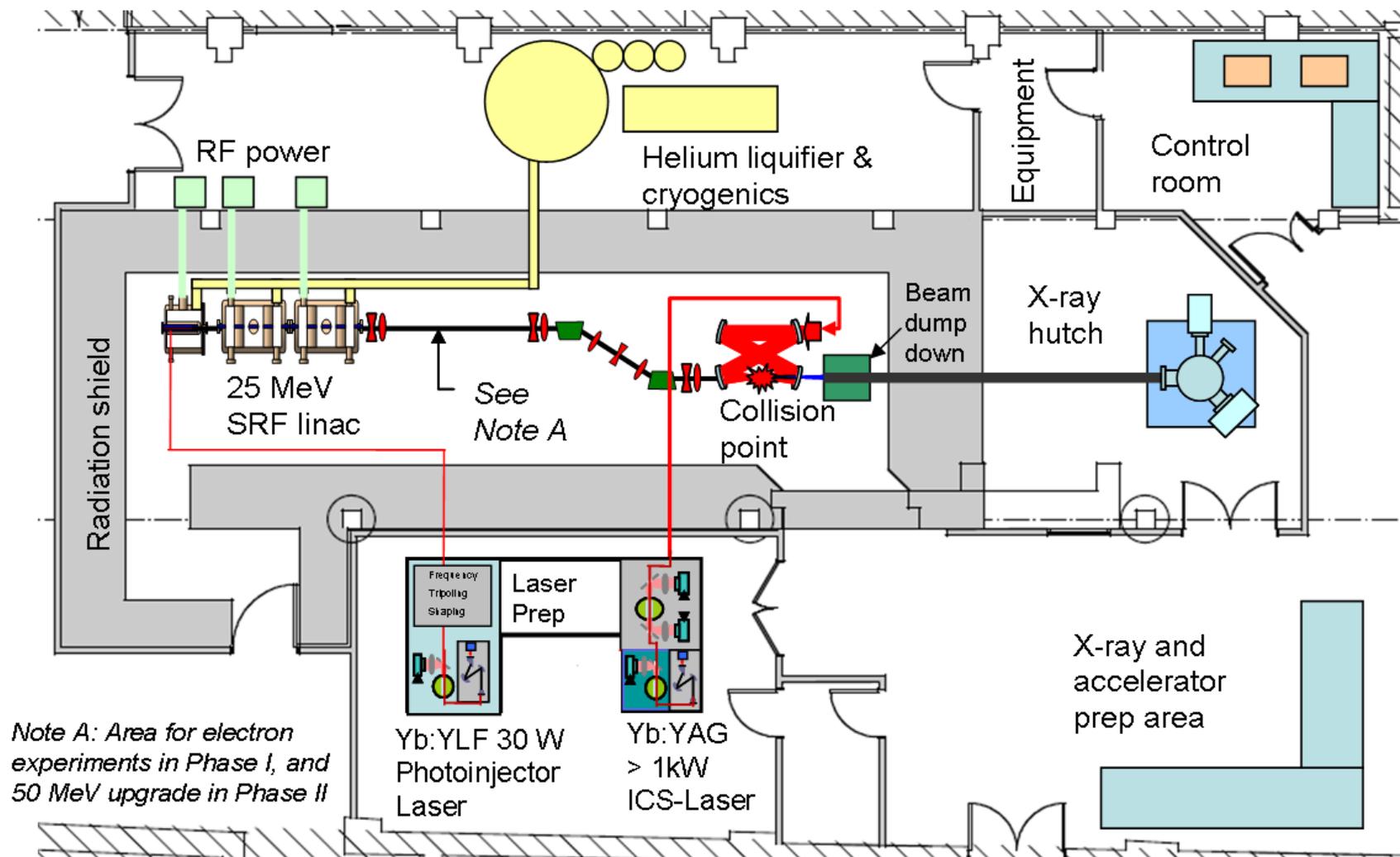
Flatness Comparison



4rd Generation X-Ray Source



4rd Generation X-Ray Source



4rd Generation X-Ray Source

- What do we want?**

-X-Ray specs



Parameter	Quantity	Unit
X-ray energy	Up to 12	keV
Photons/bunch	1.6×10^6	
Flux	1.6×10^{14}	photon/sec
Average Brilliance	1.5×10^{15}	photon/(sec mm ² mrad ² 0.1%BW)

- What do we need?**

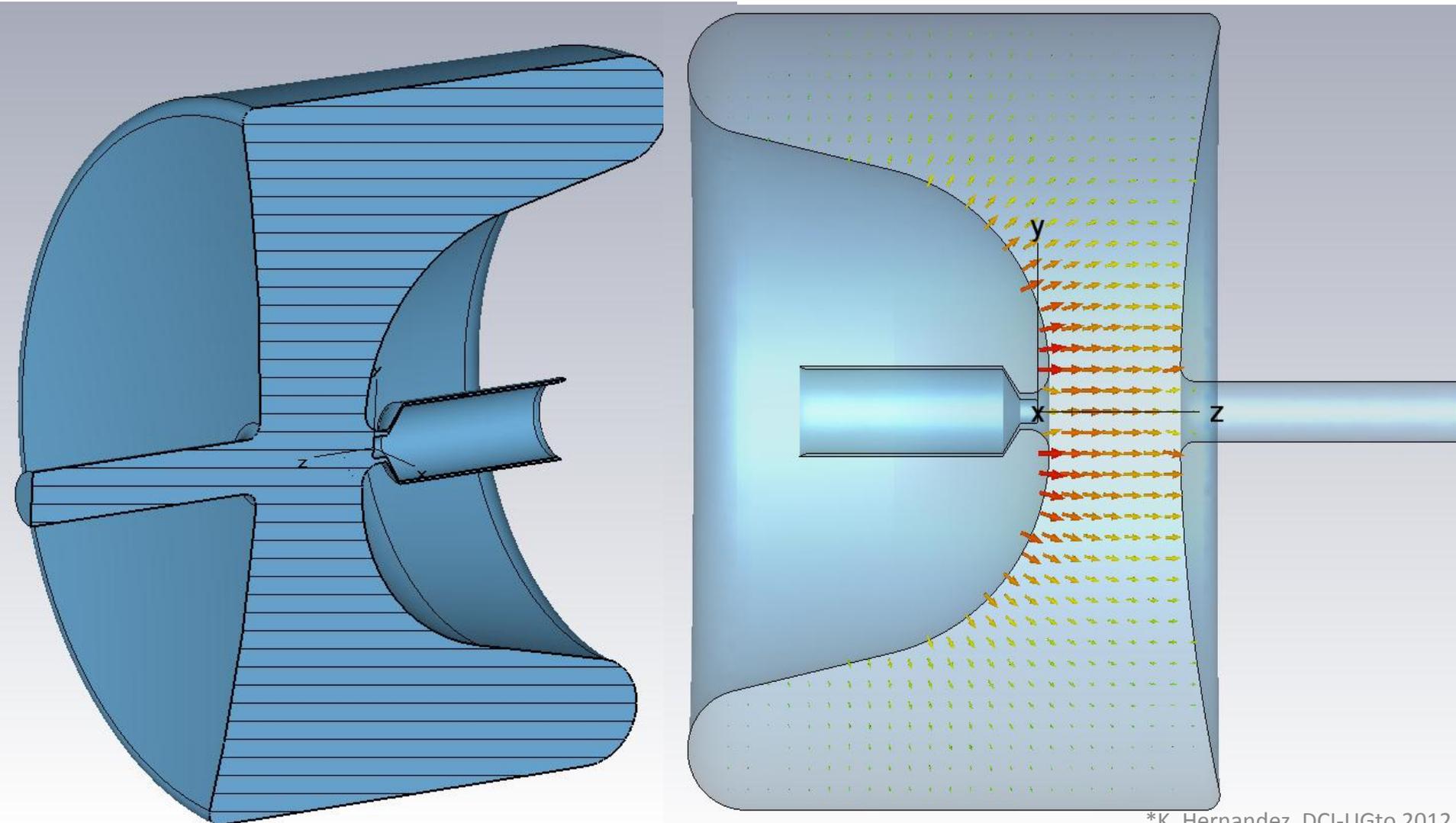
-Beam specs



Parameter	Quantity	Unit
Energy	25	MeV
Bunch charge	10	pC
Repetition rate	100	MHz
Average current	1	mA
Normalized emittance	0.1	mm-mrad
β	5	mm
FWHM bunch length	3.0(0.9)	psec(mm)
RMS energy spread	7.5	keV

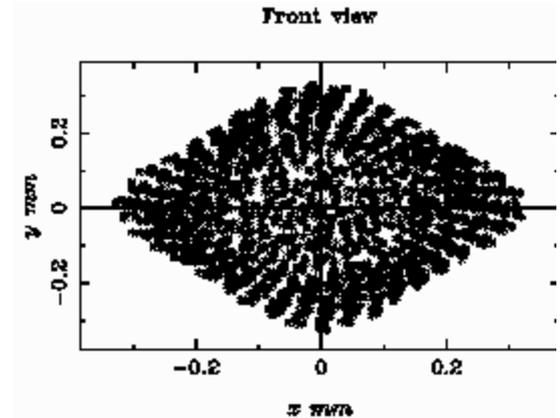
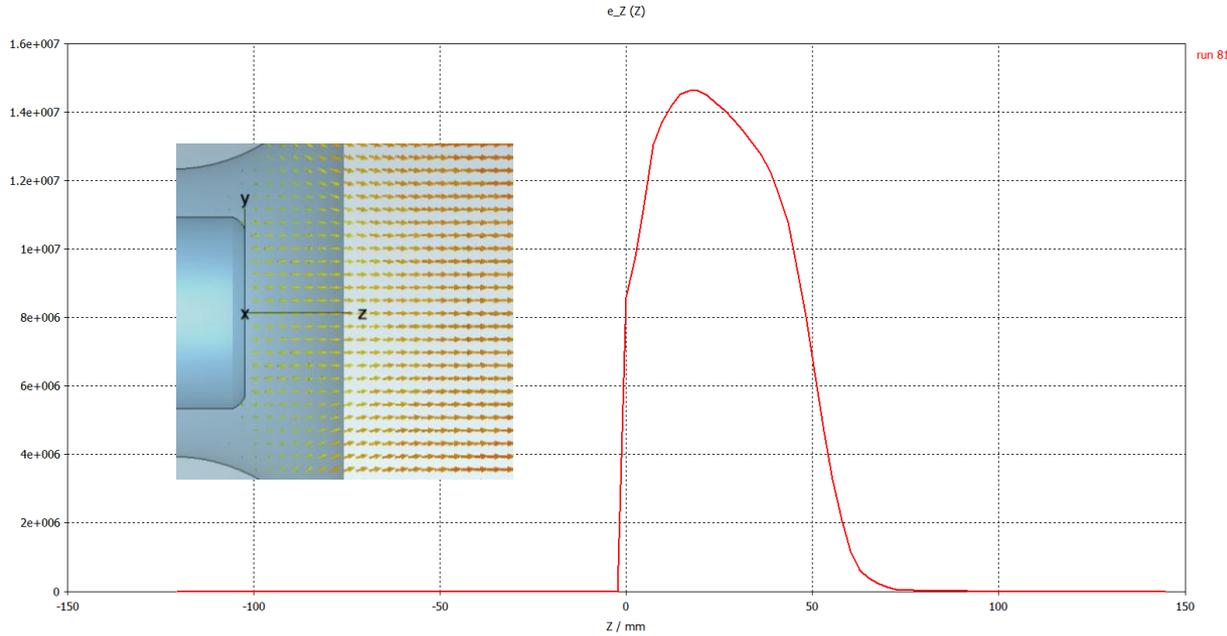


4rd Generation X-Ray Source



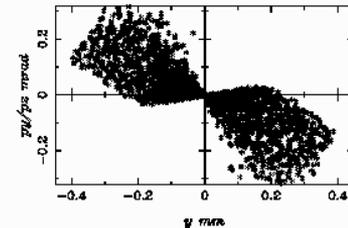
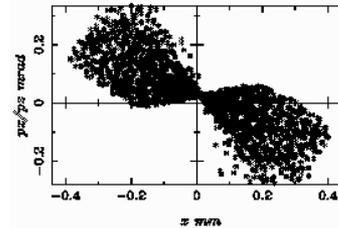


4rd Generation X-Ray Source



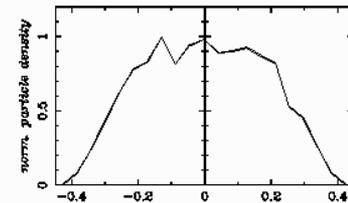
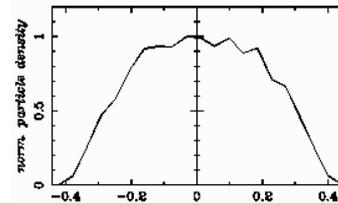
$z = 0.5000 \text{ m}$

Transverse Phase-Space



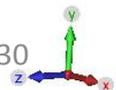
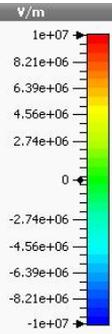
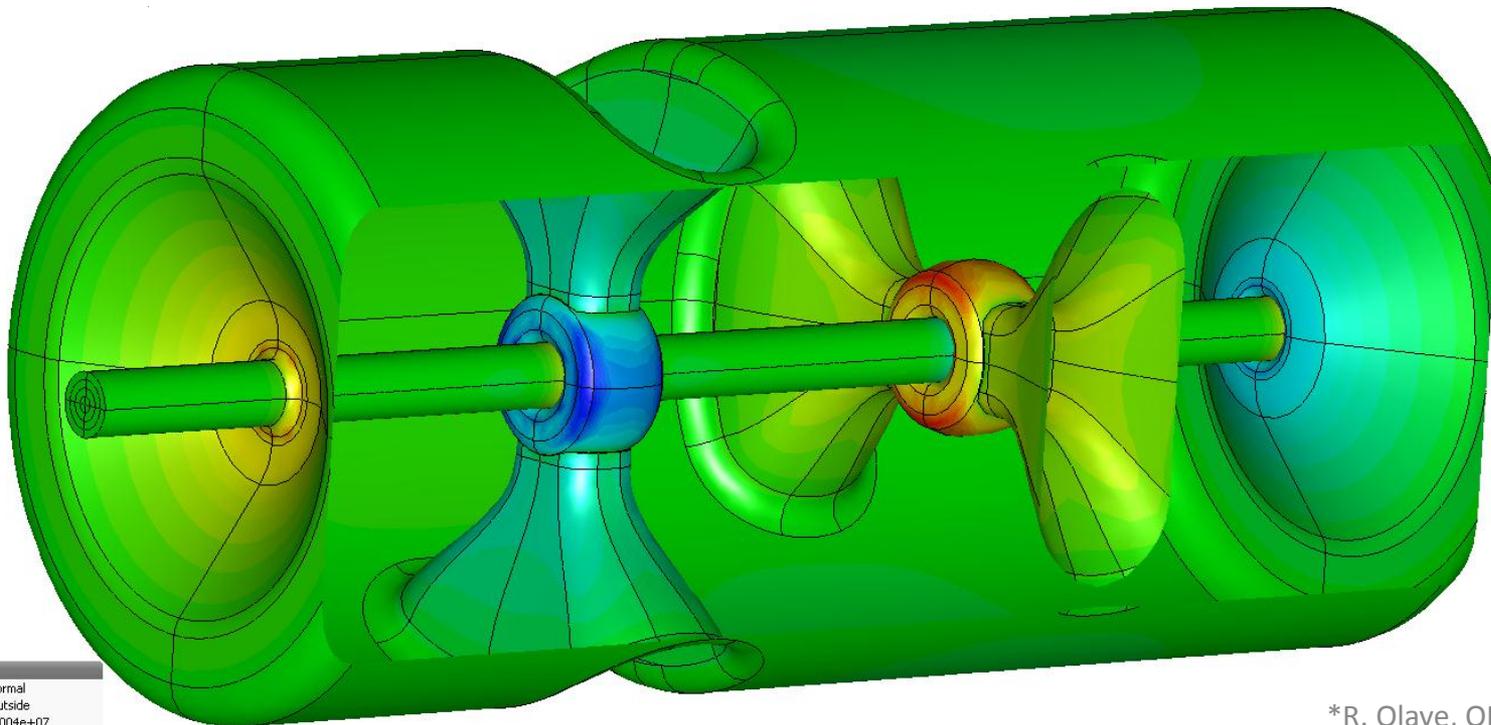
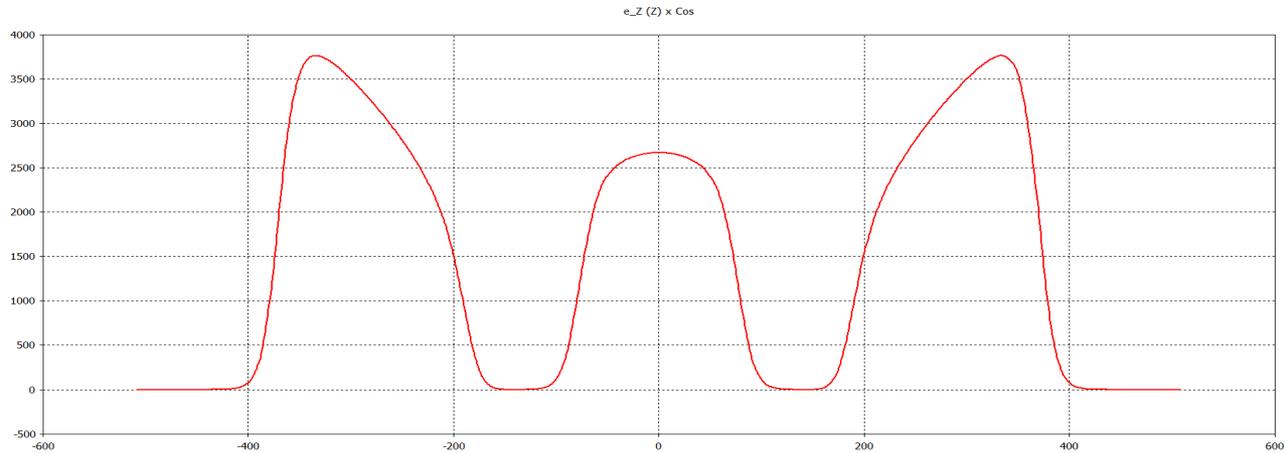
Transverse Distribution

Transverse Distribution



Vacc	Eacc	Ep over Eacc	Bp over Eacc (mT over Mv over m)
575863	3.84445e+00	5.01414	10.9625
		Bp over Ep	R over Q
		2.18631	105.483
		G	(R over Q) times (G)
		64.7645	6831.56

4rd Generation X-Ray Source





Thank you



References

- PRST-AB
 - Beam Dynamics Studies for Transverse Electromagnetic Mode-type RF Deflectors – Phys. Rev. ST Accel. Beams **15**, 022001 (2012) - S. Ahmed, et.al.
- PAC 2011 – New York, USA
 - Design of Superconducting Parallel-bar Deflecting/Crabbing Cavities with Improved Properties – J.R. Delayen, S.U. De Silva
 - Fundamental and HOM Coupler Design for the Superconducting Parallel-Bar Cavity – S.U. De Silva, J.R. Delayen
 - Multipacting Analysis of the Superconducting Parallel-bar Cavity – S.U. De Silva, J.R. Delayen
 - Beam Dynamics Studies of Parallel-Bar Deflecting Cavities – S. Ahmed, et.al.
- SRF 2011 – Chicago, USA
 - Compact Superconducting Cavities for Deflecting and Crabbing Applications – J.R. Delayen – Invited Talk
 - Designs of Superconducting Parallel-Bar Deflecting Cavities for Deflecting/Crabbing Applications – J. R. Delayen, S.U. De Silva
 - Analysis of HOM Properties of Superconducting Parallel-Bar Deflecting/Crabbing Cavities – S.U. De Silva, J.R. Delayen
 - Mechanical Study of Superconducting Parallel-Bar Deflecting/Crabbing Cavities – H. Park, S.U. De Silva, J. R. Delayen
- IPAC 2011 – San Sebastián, Spain
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 - Crab Crossing Schemes and Studies for Electron Ion Collider – S. Ahmed, et.al.

References

- PRST-AB
 - Evolution and Properties of Parallel-Bar Deflecting/Crabbing Cavities – S.U. De Silva, J.R. Delayen
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 - Design and Development of Superconducting Parallel-bar Deflecting/Crabbing Cavities – S.U. De Silva, J.R. Delayen
 - Characteristics and Fabrication of a 499 MHz Superconducting Deflecting Cavity for the Jefferson Lab 12 GeV Upgrade – H. Park, S.U. De Silva, J. R. Delayen
 - Engineering of a Superconducting 400 MHz Crabbing Cavity for the LHC HiLumi Upgrade – D. Gorelov, T. Grimm (Niowave, Inc., Lansing, Michigan), S.U. De Silva, J.R. Delayen
 - RF Modeling Using Parallel Codes ACE3P for the 400-MHz Parallel-Bar/Ridged-Waveguide Compact Crab Cavity for the LHC HiLumi Upgrade – Z. Li, L. Ge (SLAC, Menlo Park, California), J.R. Delayen, S.U. De Silva
 - Simulation of a TEM-mode Crab Cavity in the SPS – H.J. Kim, T. Sen (Fermilab, Batavia), K. Li (Stony Brook University, Stony Brook)
 - Impedance Budget for MEIC Electron Ring – S. Ahmed et.al.
- LINAC 2012 – Tel Aviv, Israel
 - Compact Superconducting Crabbing and Deflecting Cavities – S.U. De Silva – Invited Talk
 - Multipole Field Effects of Parallel-Bar Deflecting/Crabbing Cavities – S.U. De Silva, J.R. Delayen

Acknowledgements

- Terry Grimm (Niowave)
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- Christopher Hopper (ODU)
- Kirsten Deitrick (ODU)
- Randika Gamage (ODU)
- **Karim G. Hernández (DCI-Ugto)**



Extras

Preliminary Tests

- For the cavity after removing $150 \mu\text{m}$ etch with standard BCP solution:

$$Q_0 = \frac{G}{R_s} \approx 3 \times 10^8 \text{ (measured 4K)}$$

- Geometrical factor:

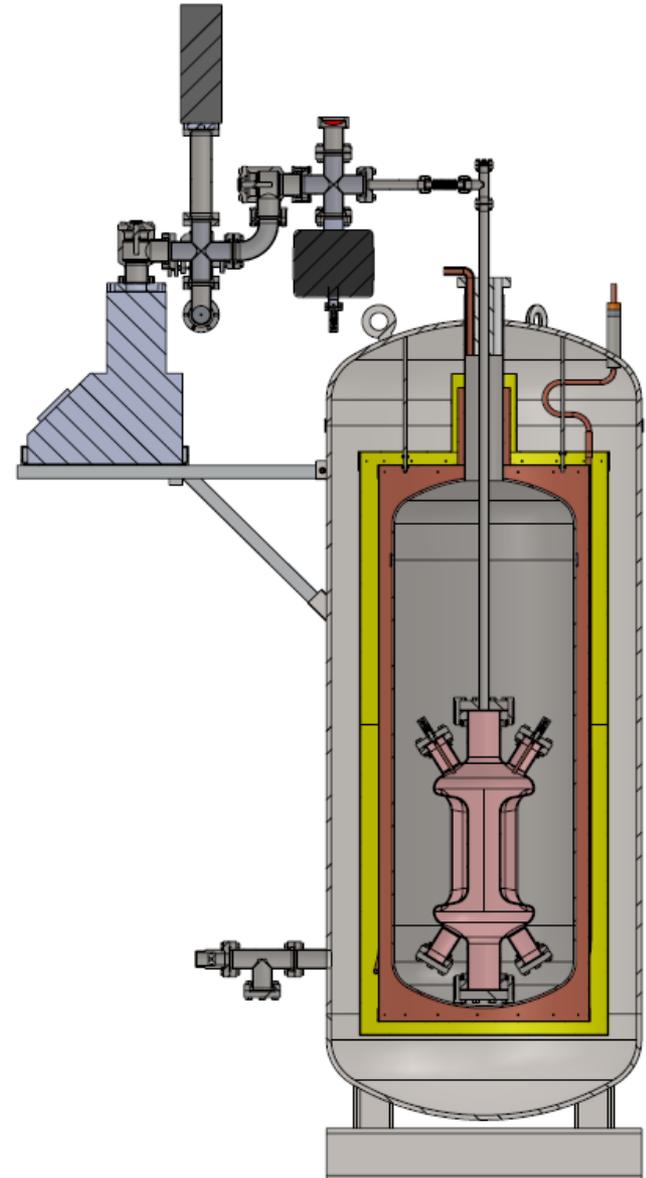
$$G = 131.4 \Omega \text{ (design)}$$

- Now, for the shunt impedance:

$$R_s = 438 \text{ n}\Omega$$

- For the power dissipated:

$$P_{dis} = 10 \text{ W (measured 4K)}$$



Preliminary Tests

- And so, for $R_T = \frac{V_T^2}{P_{dis}}$ (deflecting voltage):

$$R_T R_S = 1.65 \times 10^4 \Omega^2 \text{ (design)}$$

$$R_T = 37.67 \times 10^9 \Omega$$

- We can estimate the deflecting Voltage:

$$V \sim 0.6 \text{ MV}$$

- Using this we recalculate:

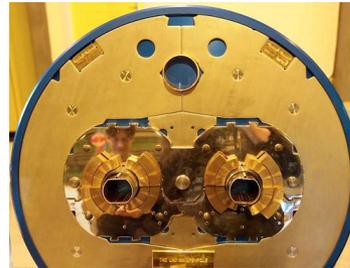
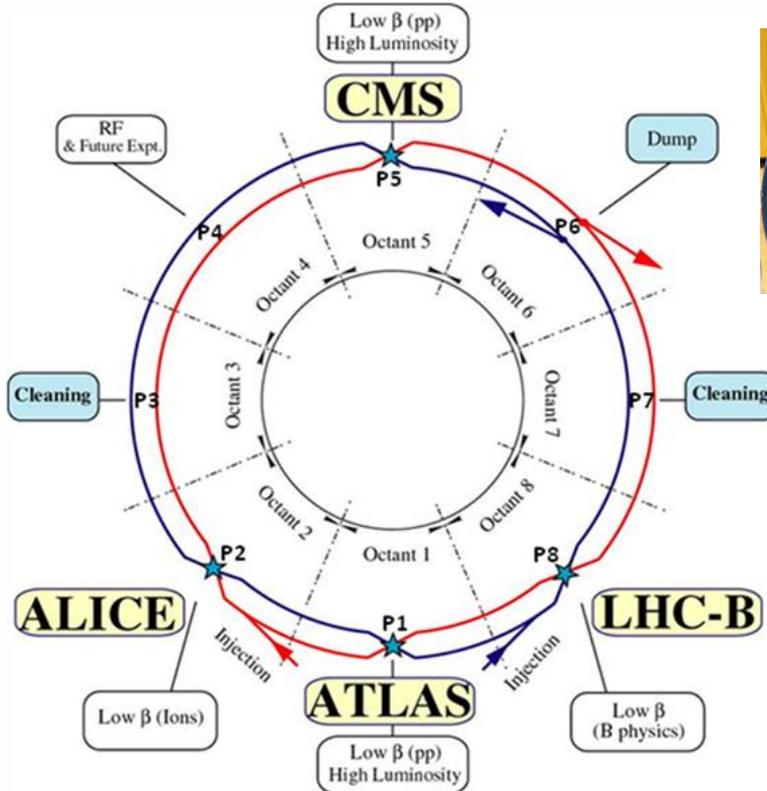
$$E_p = 13.35 \text{ MV/m}$$

$$B_p = 27.93 \text{ mT}$$



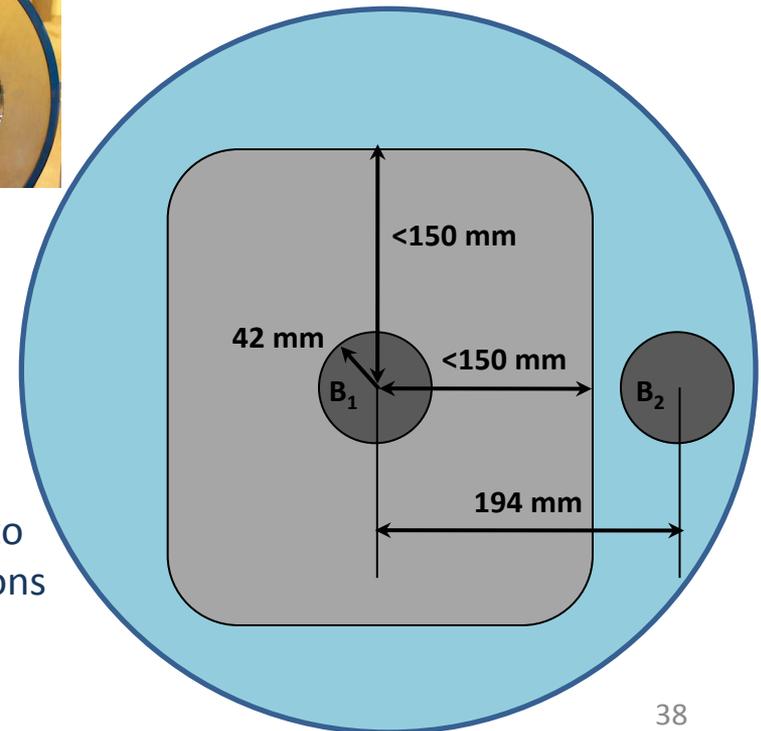
RF Crab Cavity Requirements

- Local scheme requires crab cavities on either side of the interaction point (IP)
- Requires vertical and horizontal crabbing at the two interaction points (IP1 and IP5)
- Operating rf frequency – 400 MHz
- Transverse voltage requirement - 10 MV per beam per side



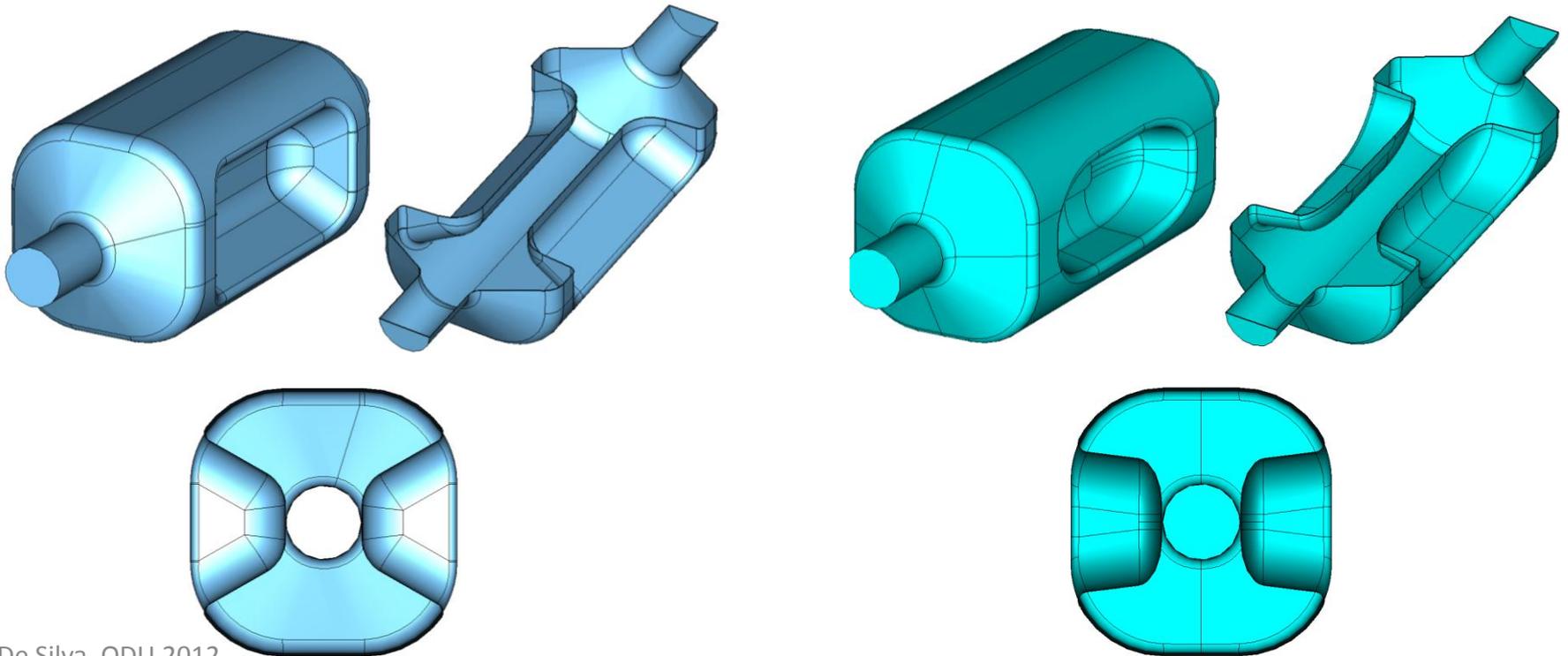
27 km @1.9K to accelerate protons to 7TeV

Dimensional Constraints



ODU/SLAC 400 MHz Square Cavity Options

- Designs are fairly similar in structure and properties
- Final design depends on final specifications
 - Field uniformity
 - Impedance budget



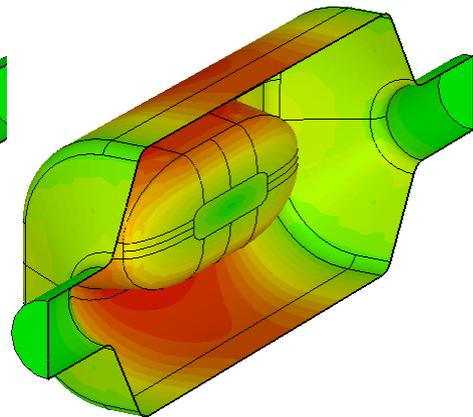
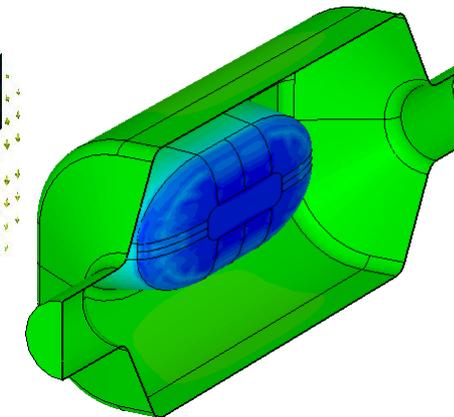
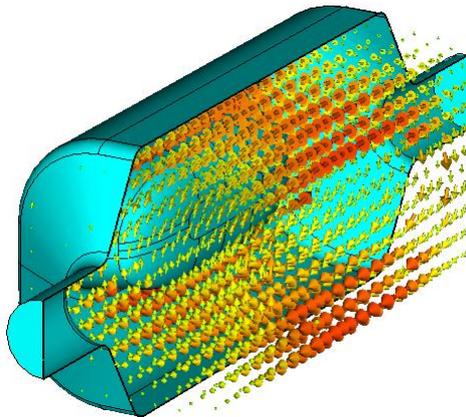
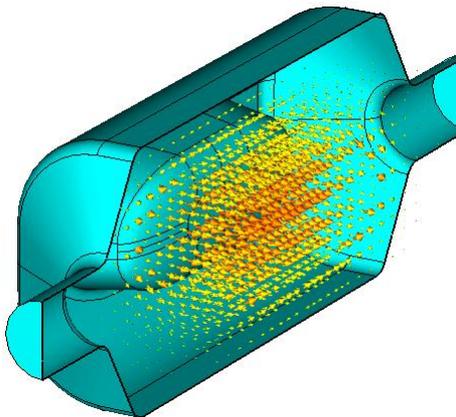
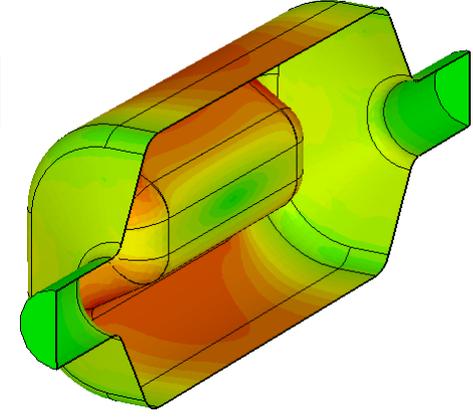
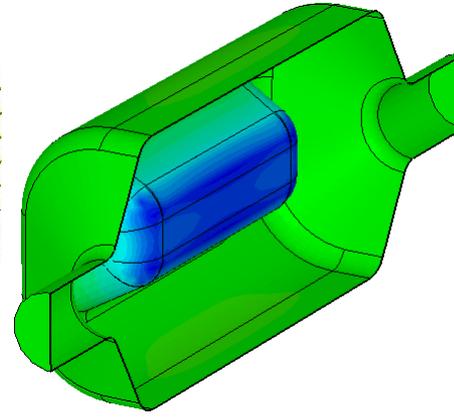
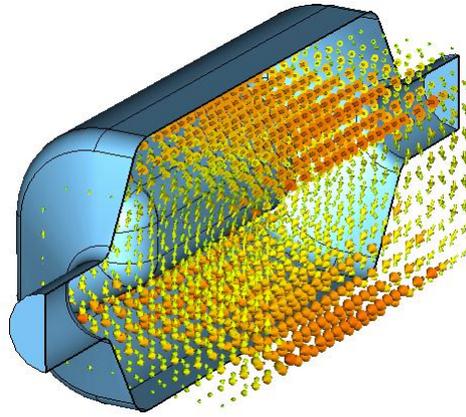
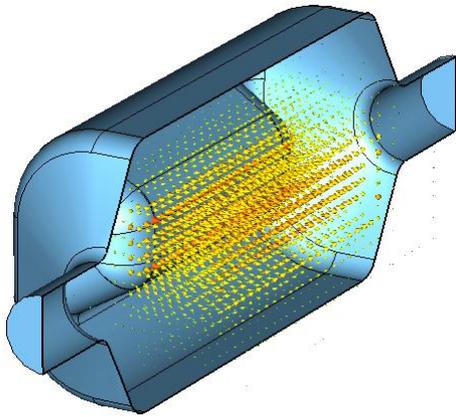
Field Distribution / Surface Fields

E Field

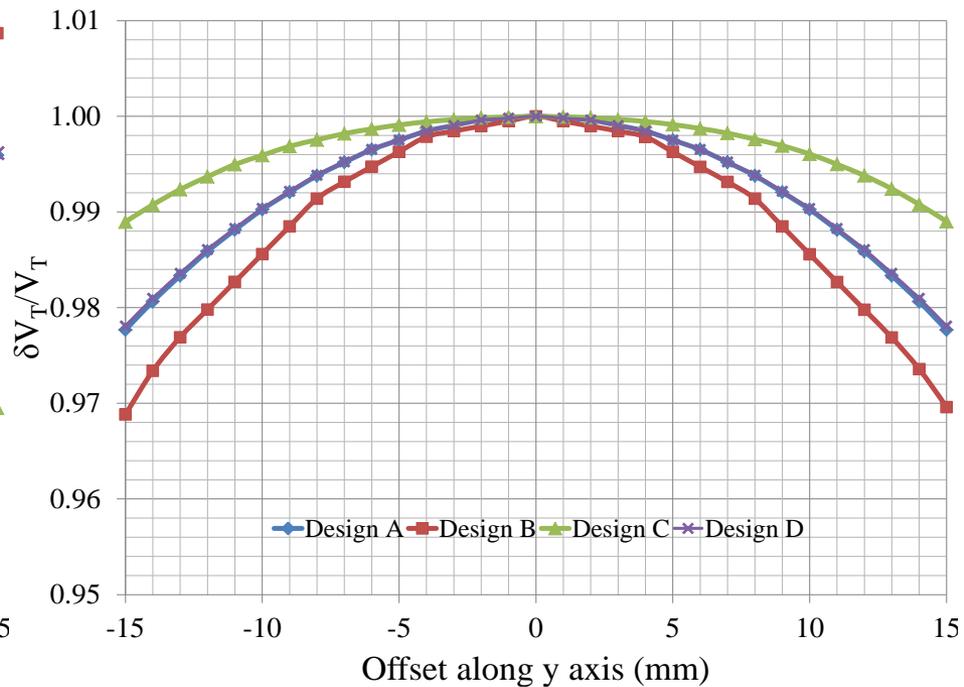
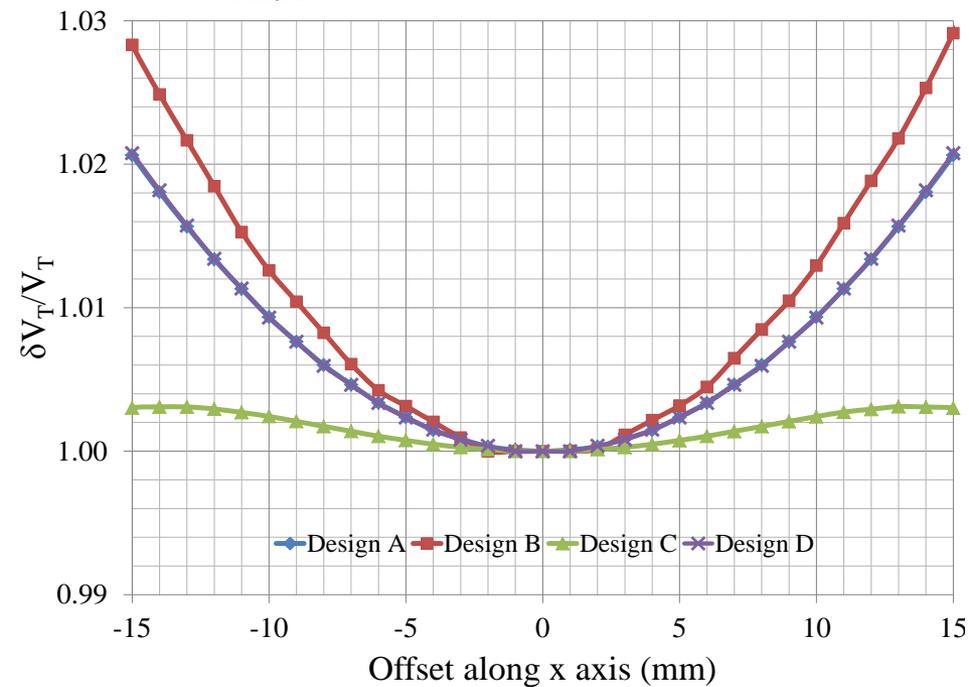
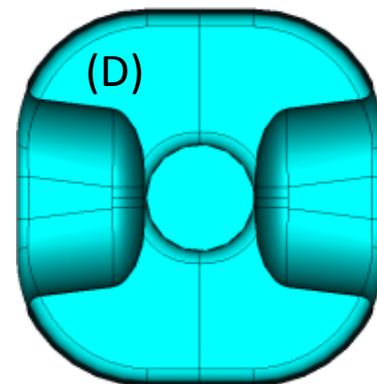
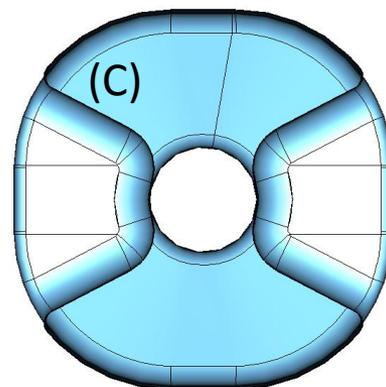
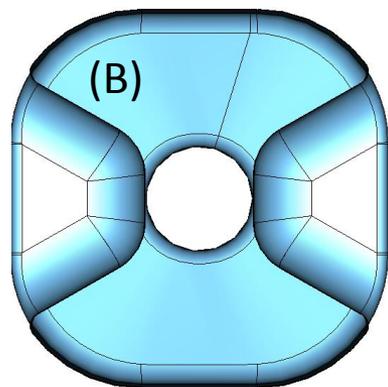
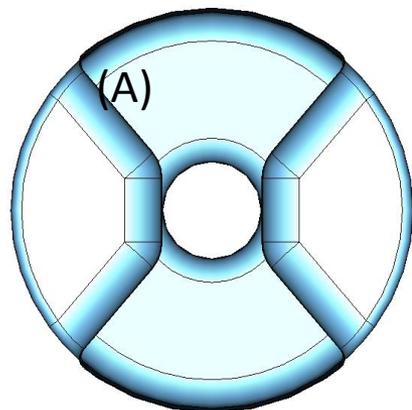
H Field

Peak E Field

Peak H Field



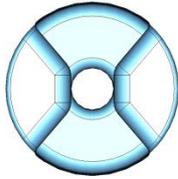
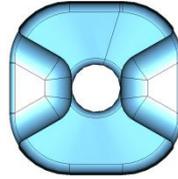
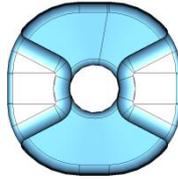
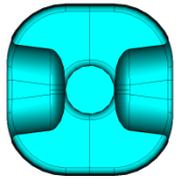
Field Non-Uniformity



Power Dissipation

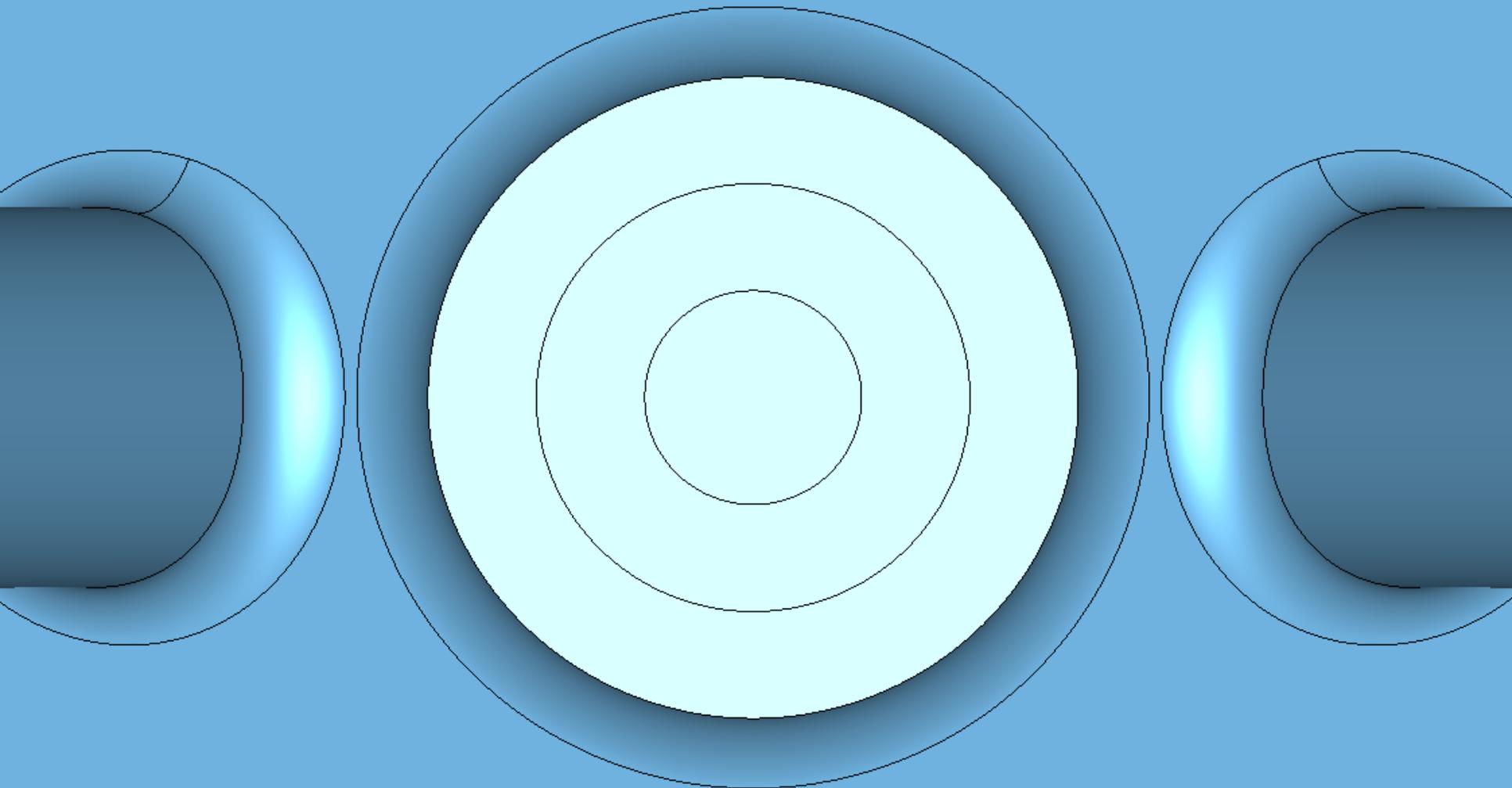
- Surface resistance of Nb at 400 MHz
 - 4.5K: 95 nΩ → 105 nΩ
 - 2K: 1.3 nΩ → 10 nΩ

$$P = \frac{V^2}{(QR_s)(R/Q)} R_s$$

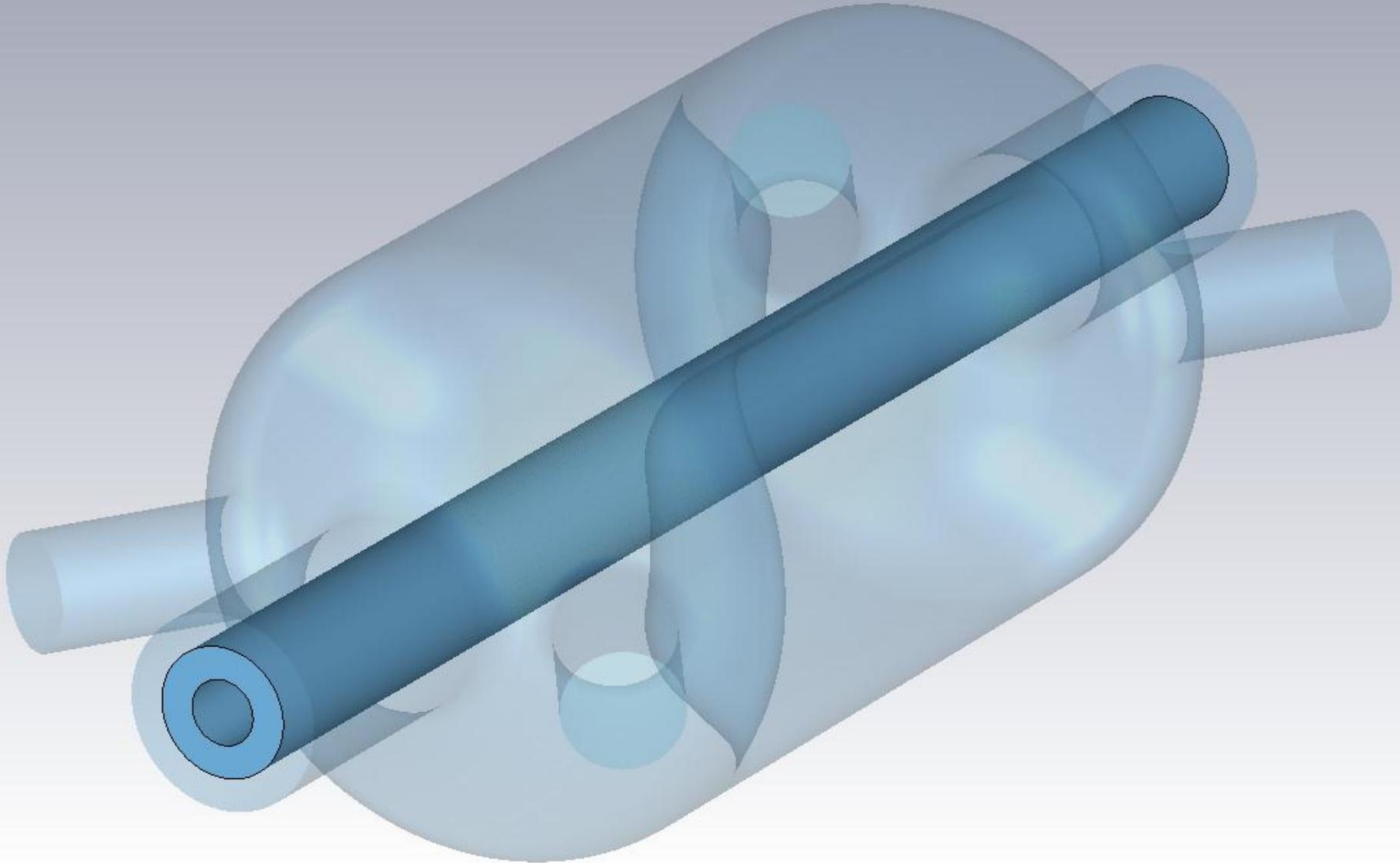
Parameter					Unit
Deflecting voltage (V_T^*)	0.375	0.375	0.375	0.375	MV
Peak electric field (E_p^*)	3.82	3.86	4.23	3.75	MV/m
Peak magnetic field (B_p^*)	7.09	6.9	7.69	6.85	mT
B_p^* / E_p^*	1.86	1.79	1.82	1.83	mT / (MV/m)
E_p at 3 MV	30.6	30.9	33.8	30.0	MV
B_p at 3 MV	56.7	55.2	61.5	54.8	mT
E_p at 5 MV	51.3	51.5	56.4	50.0	MV
B_p at 5 MV	94.5	92.0	102.5	91.3	mT
$R_T R_S$	3.7×10^4	3.6×10^4	3.7×10^4	5.1×10^4	Ω^2
P at 4.5K at 3 MV / 5 MV	25.5 / 70.9	26.3 / 72.9	25.5 / 70.9	18.5 / 51.5	W
P at 2K at 3 MV / 5 MV	2.4 / 6.8	2.5 / 6.9	2.4 / 6.8	1.8 / 4.9	W
At $E_T^* = 1$ MV/m					

Multipole Expansion

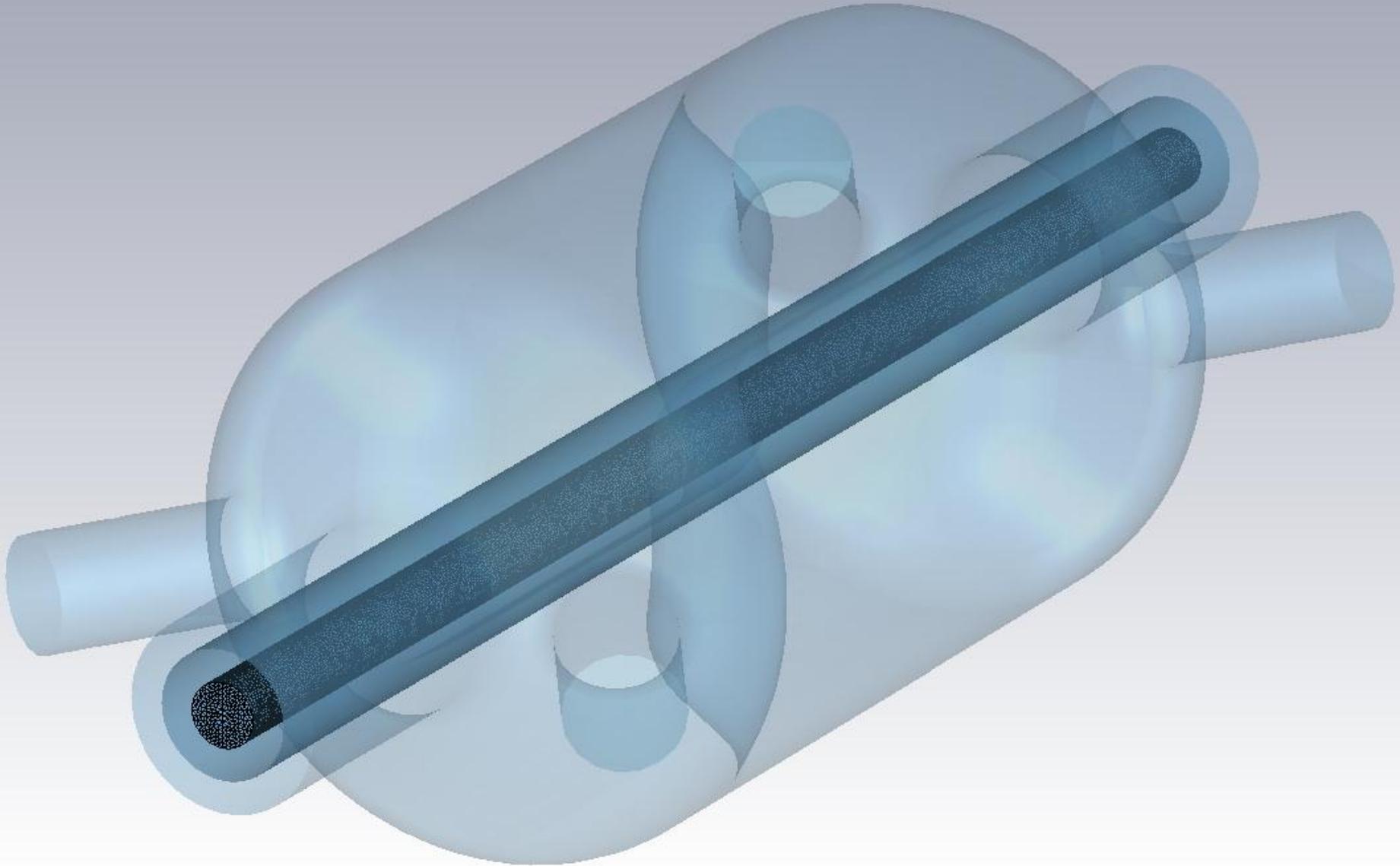
$$E(r, \phi, z) = \sum_{\mu} E_{\mu}(r, z) \cos(\mu\phi)$$



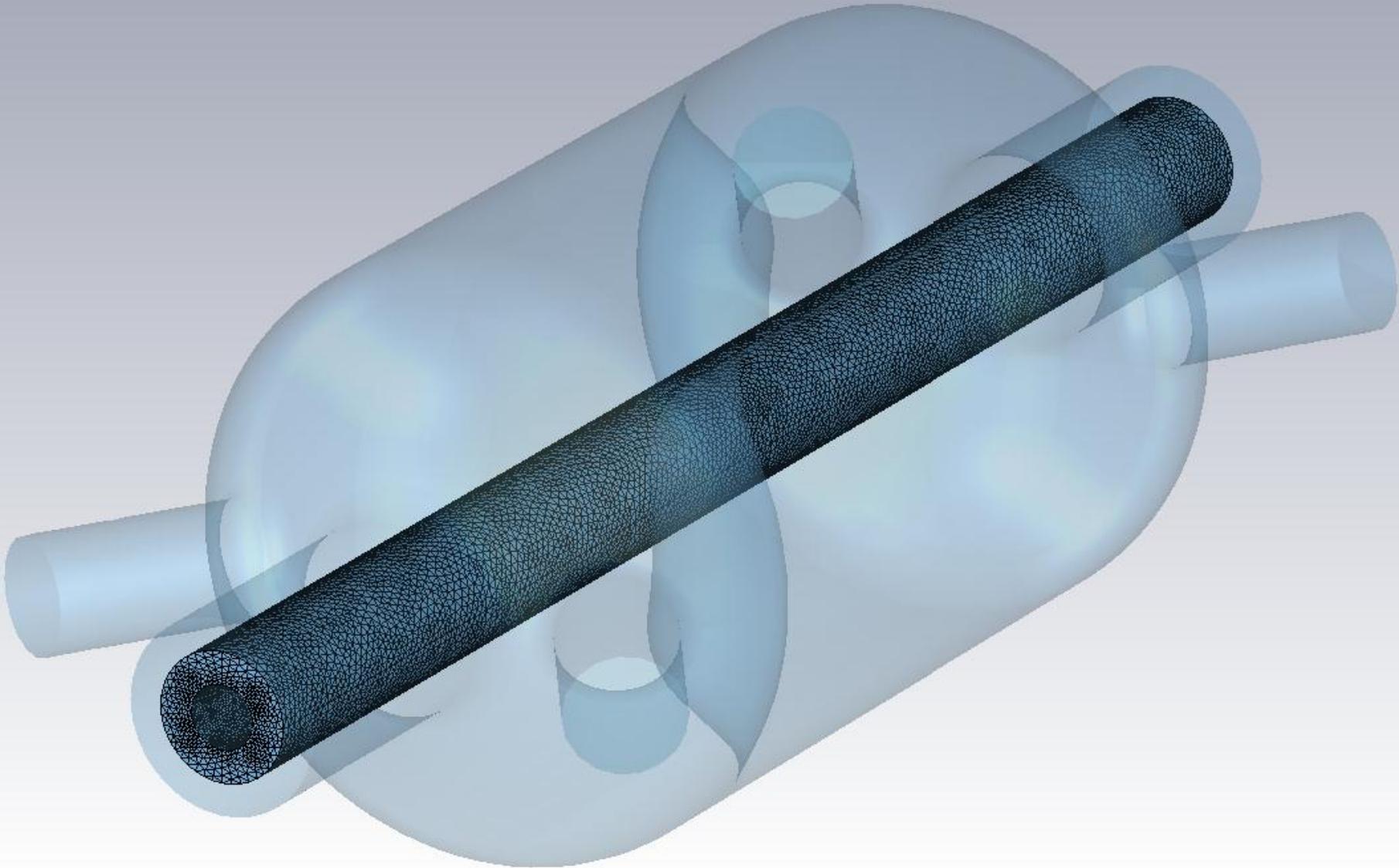
Multipole Expansion



Multipole Expansion

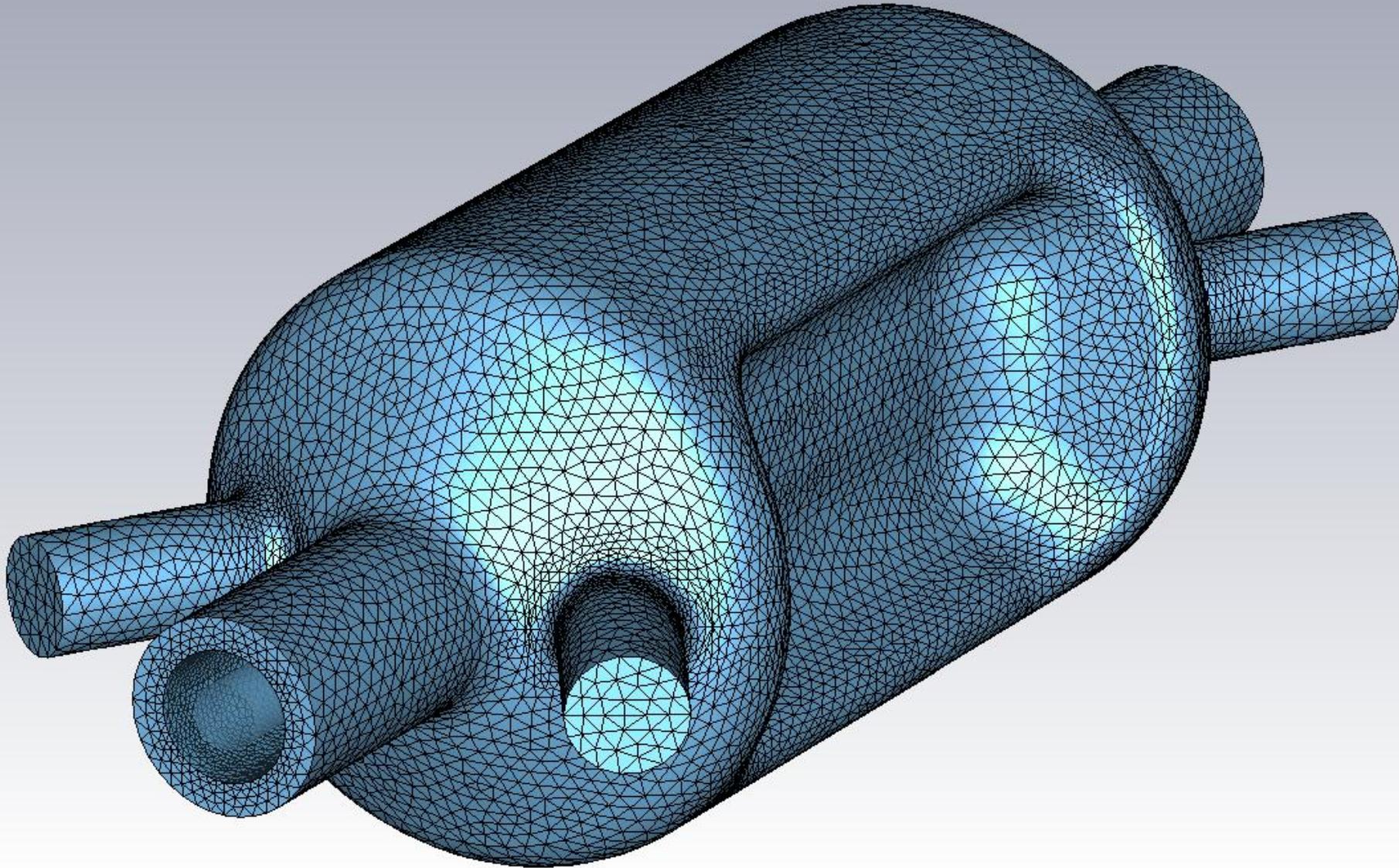


Multipole Expansion



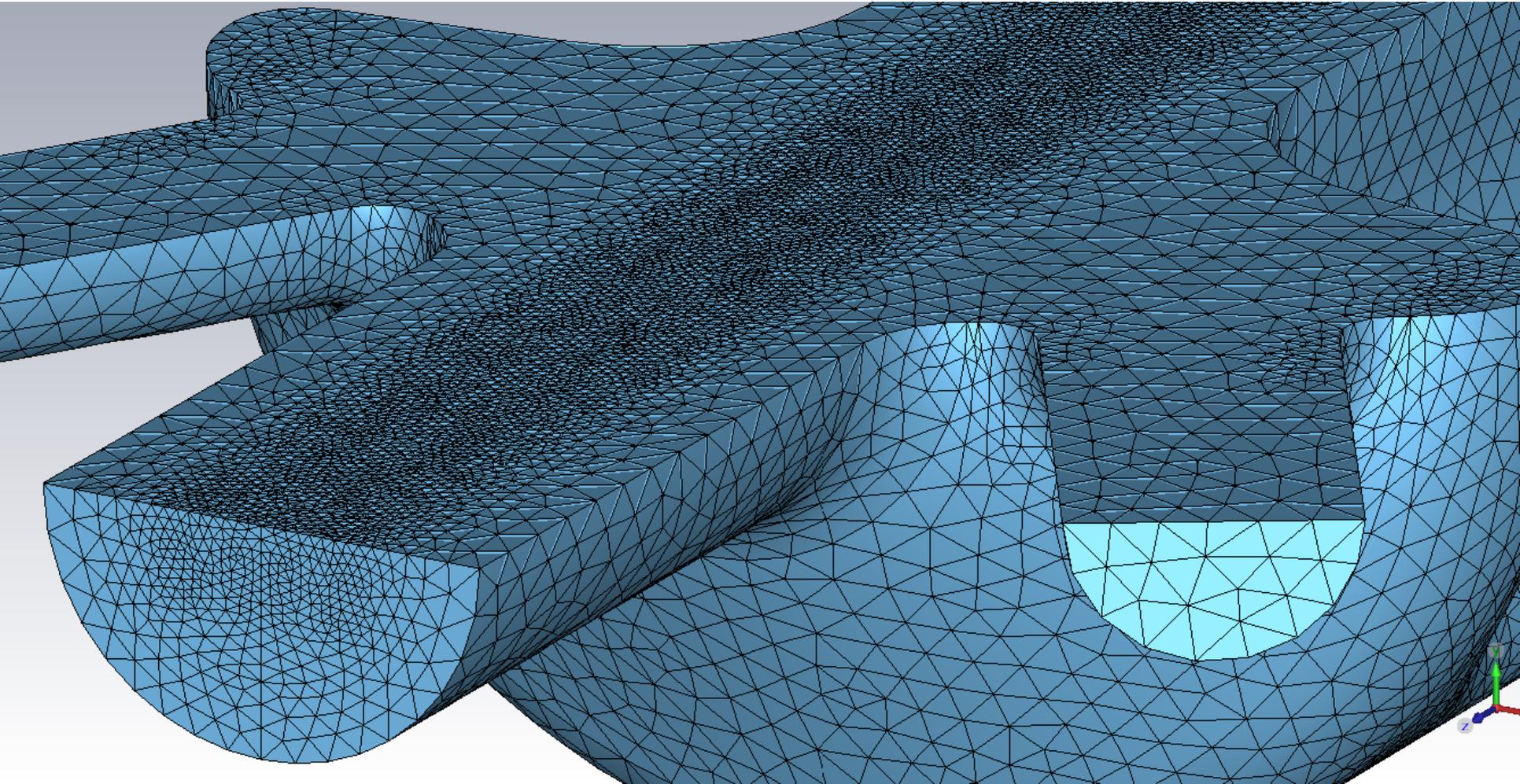


Multipole Expansion



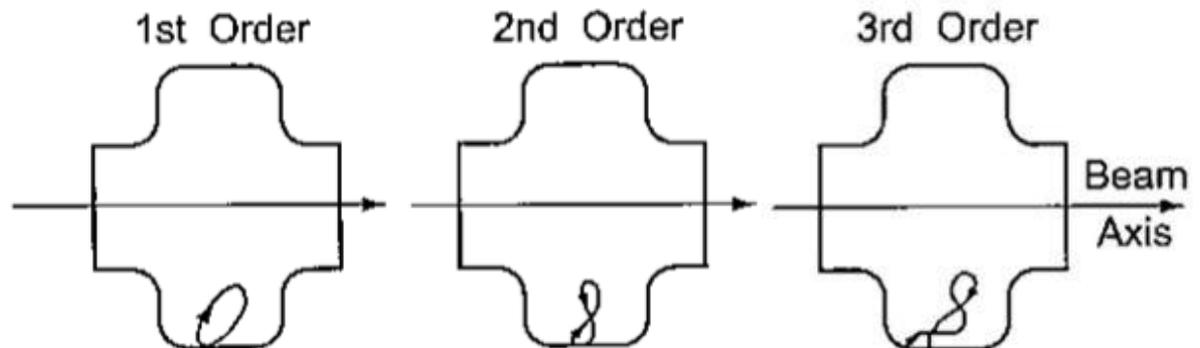


Multipole Expansion



Multipacting

- Multipacting mechanism:
 - Electron emitted from a surface due to: cosmic ray, photoemission, or field emission.
 - It is accelerated by the RF fields, impacts a wall again, and may produce secondary electrons.
 - Secondary electrons are accelerated and, upon impact, produce another electrons.
 - As a result, the avalanche of electrons may be generated.

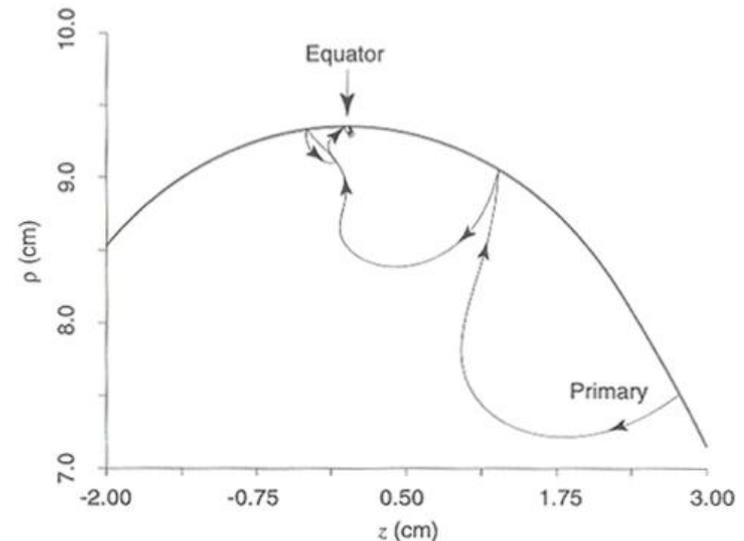
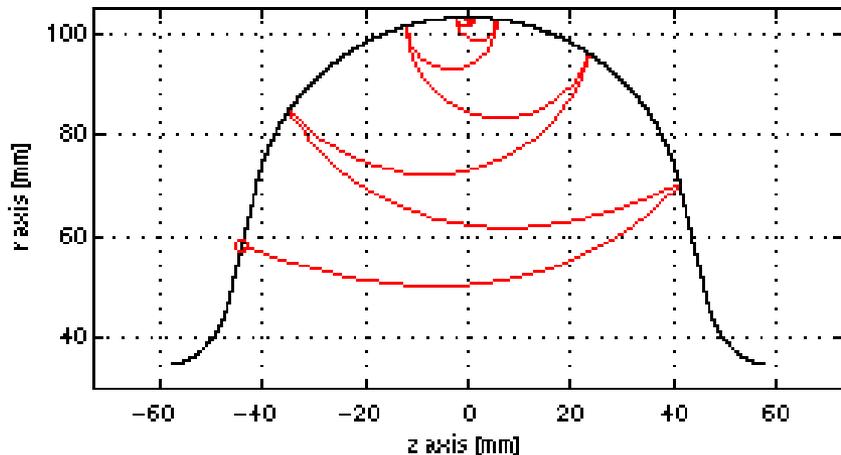


Multipacting

- RF power loss due to multipacting electrons
 - The undesirable multipacting electrons absorb the RF power.
- One mechanism of thermal breakdown in superconductor
 - The electrons collide with cavity walls.
 - The collisions lead to a large temperature rise.
 - Temperature rise causes thermal breakdown in superconductor.

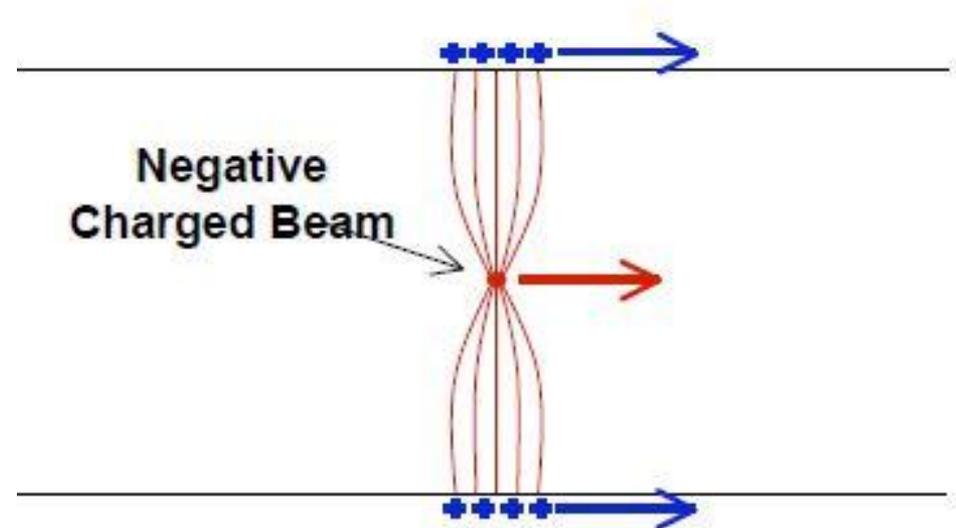
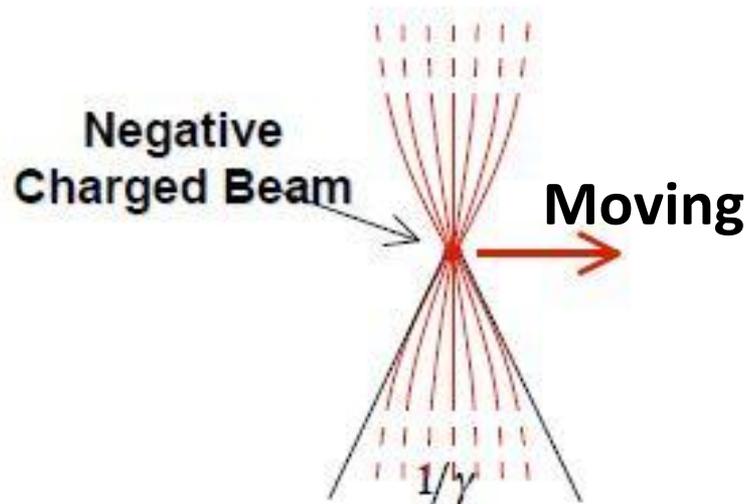
How to avoid Multipacting (Elliptical Shape)

- The multipacting electrons drift to the equator.
- At the equator, E_{\perp} vanishes.
- The electrons do not gain any energy.



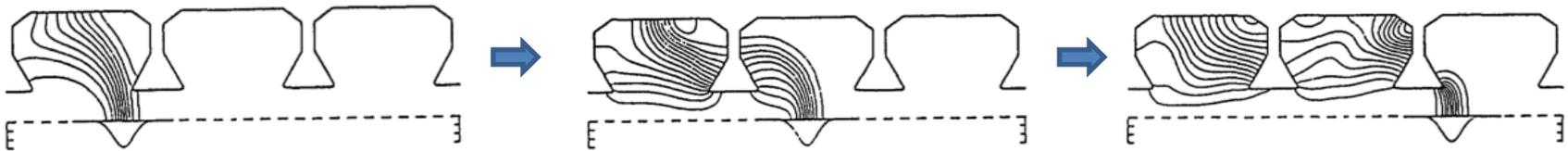
Wakefields

- Electromagnetic field of a relativistic particle
 - In the lab frame, the electric field of a relativistic particle is transversely confined within a cone of aperture of $\sim 1/\gamma$.

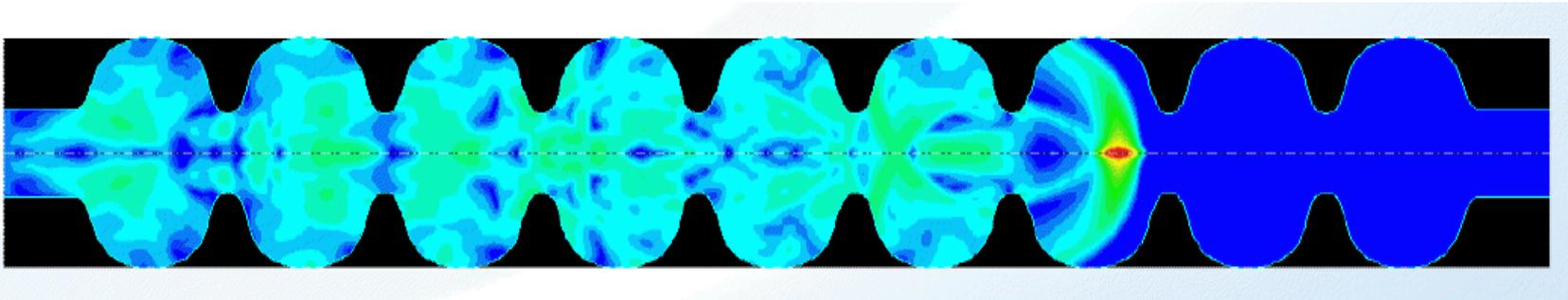


Electric Field

- Wakefield: Charged particles interact with surroundings and leave wakefields behind.



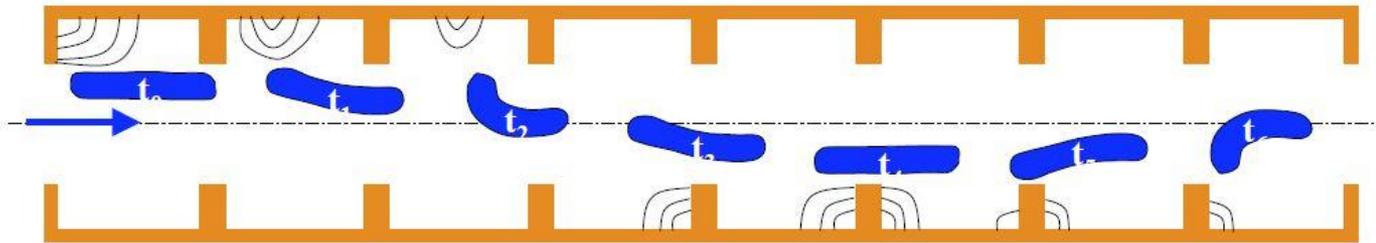
Numerically calculated electric wakefields by an ultra-relativistic Gaussian bunch



- The wakefields manifest themselves as excitations of the resonant modes in the cavity.

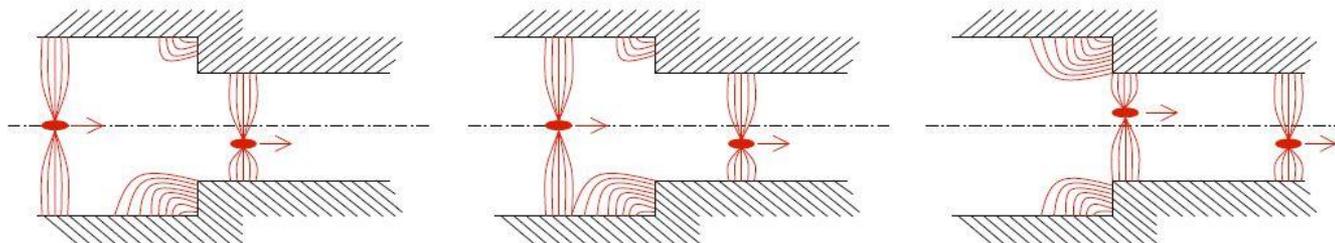
Beam Instabilities

- Single bunch instability: Particles in the tail can interact with wakefields due to particles in the head.



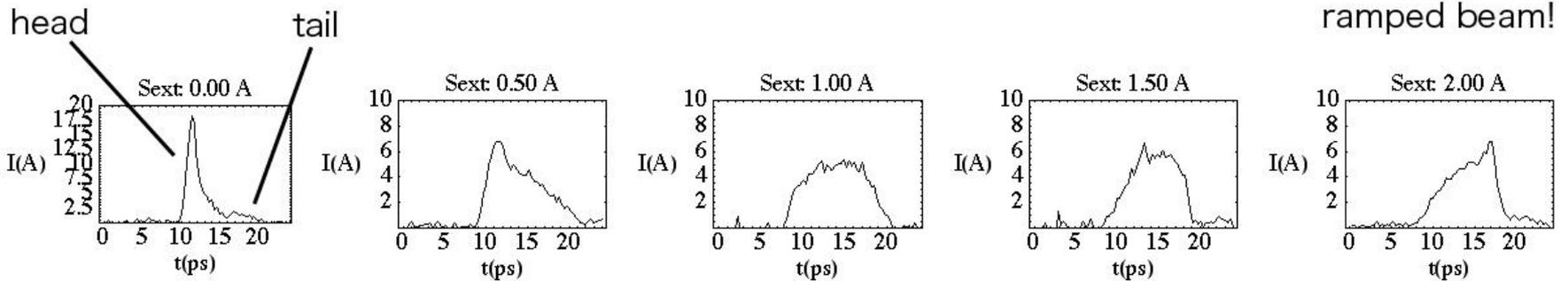
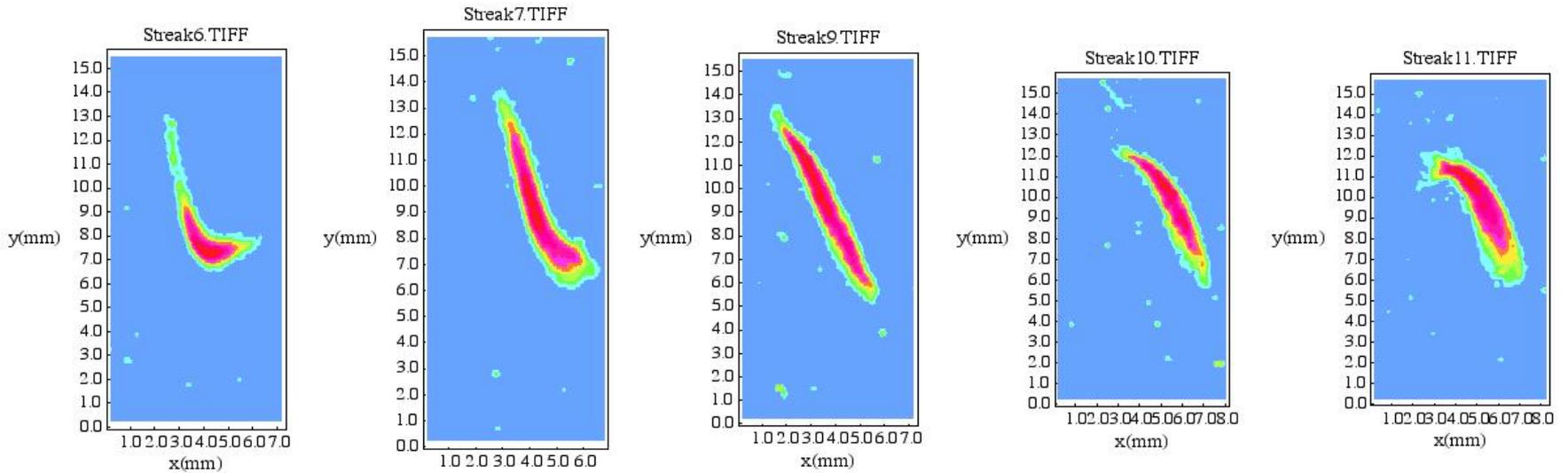
Snapshots of a single bunch traversing a SLAC structure

- Multibunch instability: Trailing bunches can interact with wakefields from leading bunches to generate multibunch instability.





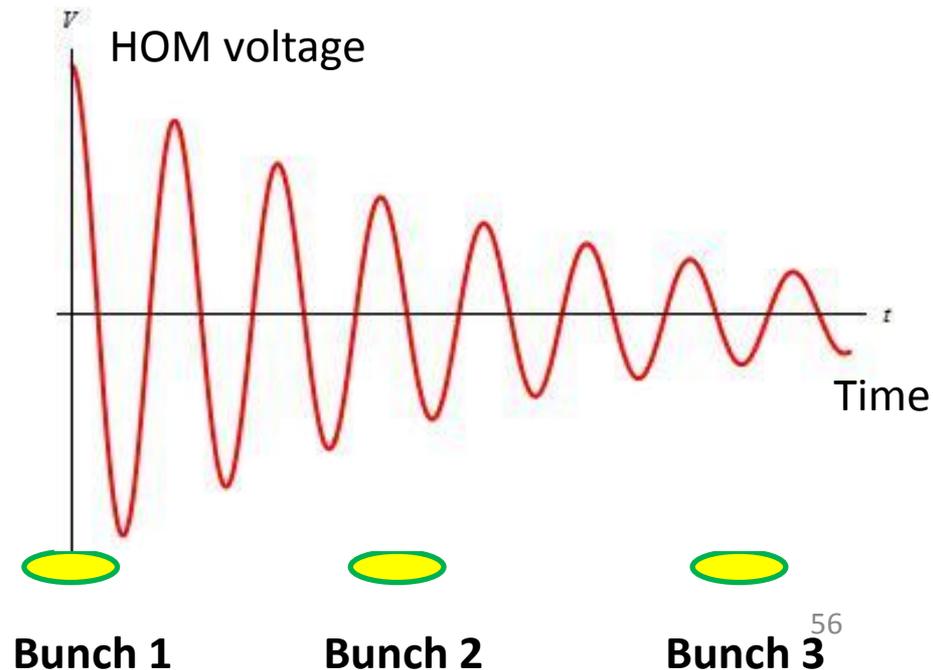
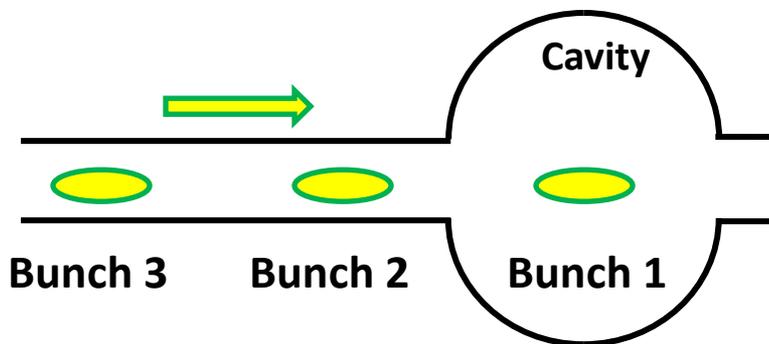
Transversal Cross Section



ramped beam!

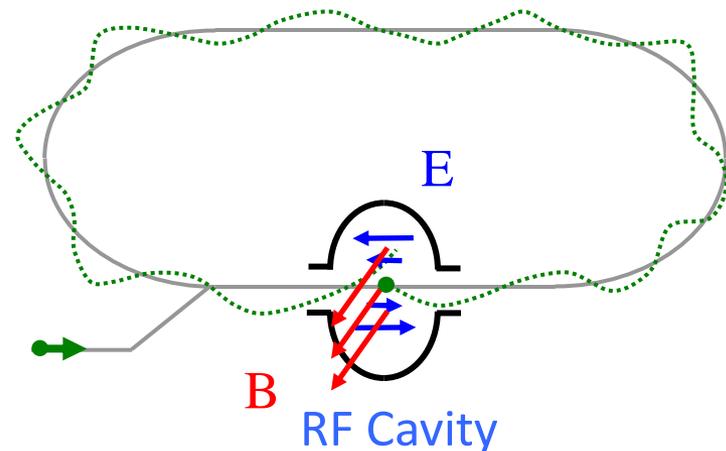
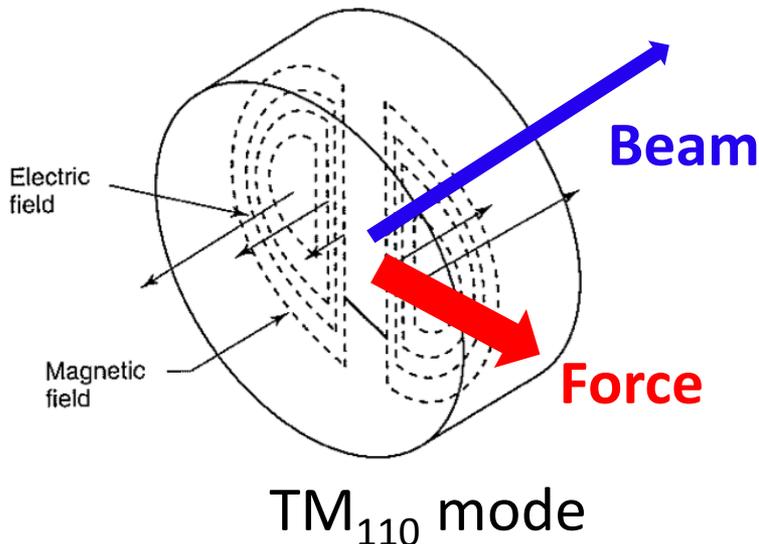
Beam Instability by HOMs

- A particle bunch excites HOMs which oscillate and decay by the cavity wall resistance.
- The trailing bunches or the same bunch on the next revolution see the HOMs oscillating in the cavity.
- The excited HOMs can be strong enough to cause instabilities on beam.



Multipass Beam Instability

- A positive feedback between the recirculated beam and the HOM which kicked the beam on the previous pass
 - A positive feedback enhances the HOM field.
 - The enhanced HOM kicks the next bunch harder.
- Beam breakup (BBU)
 - Exponential increase of the HOM field
 - Beam loss if transverse displacement > physical aperture



Higher Order Modes

- Higher Order Modes (HOMs) – Parasitic modes present in a cavity other than the fundamental mode of operation
- For a beam passing through the cavity, one or more of these modes gets activated due to the interaction with the charged particles, generating wake fields that act upon the beam in return

- Longitudinal [R/Q]

$$\left[\frac{R}{Q} \right] = \frac{|V_z|^2}{\omega U} = \frac{\left| \int_{-\infty}^{+\infty} \vec{E}_z(z, x=0) e^{\frac{j\omega z}{c}} dz \right|^2}{\omega U}$$

- Transverse [R/Q]

- Direct Integral Method

$$\left[\frac{R}{Q} \right]_T = \frac{|V_T|^2}{\omega U} = \frac{\left| \int_{-\infty}^{+\infty} \left[\vec{E}_x(z, x=0) + j(\vec{v} \times \vec{B}_y(z, x=0))_T \right] e^{-\frac{j\omega z}{c}} dz \right|^2}{\omega U}$$

- Using Panofsky Wenzel Theorem ($x_0=5$ mm)

$$\left[\frac{R}{Q} \right]_T = \frac{|V_z(x=x_0)|^2}{\omega U} \frac{1}{(kx_0)^2} = \frac{\left| \int_{-\infty}^{+\infty} E_z(z, x=x_0) e^{\frac{j\omega z}{c}} dz \right|^2}{(kx_0)^2 \omega U}, \quad k = \frac{\omega}{c}$$

Types of Modes

Field on Beam Axis	Type of Mode
E_x, H_y	Deflecting
E_z	Accelerating
E_y, H_x	Deflecting
H_z	Does not couple to the beam

No Lower Order Modes

HOM damping

- HOM couplers
 - extract HOMs energy.
 - have to be broadband to cover the most HOMs.
 - should not damp the accelerating mode.

